

Flow Solver Overview - PMBv1.5

- Parallel Multiblock (PMB) structured solver developed since 1996
- Solving 2D/3D steady/unsteady compressible Euler/Navier-Stokes equations
- Various turbulence models (SAE, k- $\omega$, etc.)
- Cell-centred finite-volume scheme
- Euler fluxes via Riemann solver (Roe, Osher)
- Higher-order spatial accuracy using MUSCL
- Viscous fluxes using Green-Gauss theorem
- Two halo layers to impose boundary conditions
- Fully-implicit time marching
- 2nd-order dual-time stepping for unsteady simulations
- Krylov subspace sparse iterative solver with BILU preconditioning for solving linear systems


## RSW Grids Overview

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- Inflow boundary location is 1000 inch ahead of LE
- 55 inch span
- no splitter plate
- viscous wind tunnel wall

|  | Grid points | Grid cells |
| :---: | :---: | :---: |
| Coarse | $2,321,200$ | $2,028,800$ |
| Medium | $6,597,984$ | $6,003,264$ |
| Fine | $18,632,712$ | $17,432,544$ |




Geometry and blocking files provided by Thorsten Hansen (ANSYS).

## RSW Grids Overview

- Surface mesh and typical surface pressure distribution for fine grid


176 blocks overall

## Simulated Cases

## Steady

- cases 6E23 and 6E24
- coarse, medium and fine grids (SAE model)
- coarse and medium grids (SST model)

Unsteady

- cases 6E54 and 6E56
- coarse and medium grids (SAE model)


## Steady Simulations Overview

- Osher's Riemann solver for Euler fluxes
- Turbulence model used is compressible form of Spalart-Allmaras model with Edwards' modifications (SAE), also SST model for comparison
- Run fully turbulent
- Moment centre at $\mathrm{x} / \mathrm{c}=0.46$
- Reference area for integrated loads is 24 inch x 48 inch
- CL,CD,CM include pressure and friction contributions


## Steady Results



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## Steady Results




## Steady Results

- Integrated forces and moment (CL,CM,CD)

| 6E23 | Lift | Drag | Moment |
| :---: | :---: | :---: | :---: |
| Coarse | 0.549797 | 0.047004 | 0.033167 |
| Medium | 0.540689 | 0.046688 | 0.035106 |
| Fine | 0.534424 | 0.046488 | 0.035346 |


| 6E24 | Lift | Drag | Moment |
| :---: | :---: | :---: | :---: |
| Coarse | 0.688156 | 0.075762 | -0.000897 |
| Medium | 0.684095 | 0.075505 | 0.001103 |
| Fine | 0.679196 | 0.075321 | 0.001602 |





## Steady Results - SA vs. SST

- Boundary layer velocity profile
6E23 (pnt. 626) $\quad X=11.04$ inch



## Unsteady Simulations Overview

- Unsteady runs started from converged steady case 6E23
- Forced pitching motion about $\mathrm{x} / \mathrm{c}=0.46$ at 10 Hz (6E54) and 20 Hz (6E56) with 2 degrees mean incidence and pitching amplitude of 1 degree
- Pitching motion applied via a rigid rotation of computational domain
-influence on wind tunnel wall boundary layer?
- Simulation of 8 cycles with 64 steps per cycle
- max. 50 pseudo steps per real time step
-target convergence in pseudo time is 3 orders of magnitude
-criterion: update in pseudo time scaled by change in real time
- Signal used for Fourier analysis starting from $3^{\text {rd }}$ cycle (remove transients!)


## Unsteady Results

- Magnitude and phase of CP vs. $\mathrm{x} / \mathrm{c}$ at excitation frequency $(10 \mathrm{~Hz})$




## Unsteady Results

- Magnitude and phase of CP vs. $x / c$ at excitation frequency $(10 \mathrm{~Hz})$




## Unsteady Results

- Magnitude and phase of CP vs. $\mathrm{x} / \mathrm{c}$ at excitation frequency $(10 \mathrm{~Hz})$



## Unsteady Results

- Magnitude and phase of CP vs. $\mathrm{x} / \mathrm{c}$ at excitation frequency $(10 \mathrm{~Hz})$




## Unsteady Results

- Magnitude and phase of CP vs. x/c at excitation frequency ( 20 Hz )



## Unsteady Results

- Magnitude and phase of CP vs. $\mathrm{x} / \mathrm{c}$ at excitation frequency $(20 \mathrm{~Hz})$



## Unsteady Results

- Magnitude and phase of CP vs. x/c at excitation frequency ( 20 Hz )



## Unsteady Results

- Magnitude and phase of CP vs. $\mathrm{x} / \mathrm{c}$ at excitation frequency $(20 \mathrm{~Hz})$




## Unsteady Results

- Time history of lift coefficient



## Unsteady Results

- Real and imaginary parts of CD,CM,CD

| 6E54 (10 Hz) | Lift |  | Drag |  | Moment |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Real | Imag | Real | Imag | Real | Imag |
| Coarse | 6.1936 | -1.3162 | 0.7310 | 0.0176 | -0.9866 | 0.7812 |
| Medium | 6.3108 | -1.2777 | 0.7269 | 0.0098 | -1.0097 | 0.7789 |
| Fine | -- |  |  | -- |  |  |


| 6E56 (20 Hz) | Lift |  | Drag |  | Moment |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Real | Imag | Real | Imag | Real | Imag |
| Coarse | 4.4496 | -0.9961 | 0.7401 | -0.1056 | -0.5701 | 0.7957 |
| Medium | 4.4607 | -0.9918 | 0.7306 | -0.1033 | -0.5816 | 0.8258 |
| Fine | -- |  | -- |  | -- |  |

## Future Work

- Understand differences between SAE and SST turbulence models when simulating boundary layer on wind tunnel wall.
$\rightarrow$ Does a more similar boundary layer "correct" steady shock location differences?
- For temporal convergence, double number of real time steps per cycle.

