



## INTEGRATED VEHICLE HEALTH MANAGEMENT

### ***Probabilistic fatigue damage prognosis and uncertainty management***

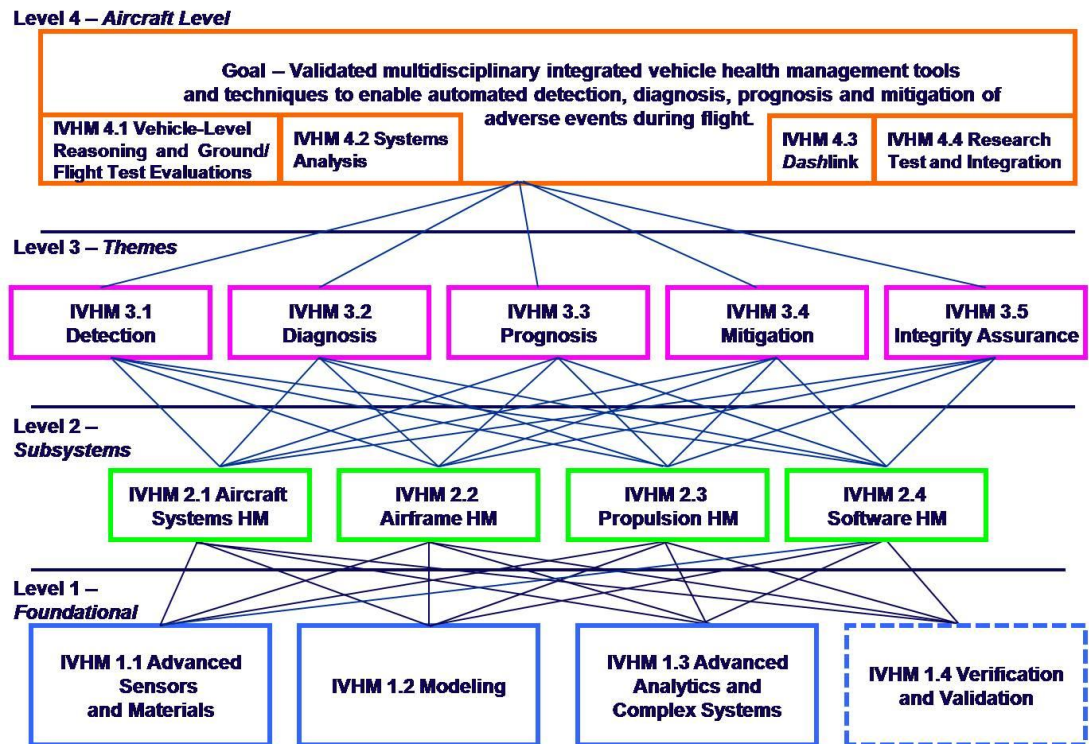
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Clarkson University***

***Sankaran Mahadevan  
Vanderbilt University***

Aviation Safety Program Technical Conference  
November 17-19, 2009  
Washington D.C.

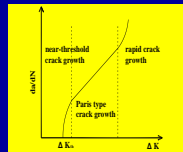
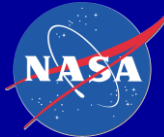
# Outline

- Problem Statement
- Background
- IVHM milestones being addressed
- Approach
- Results
- Conclusions
- Future Plans

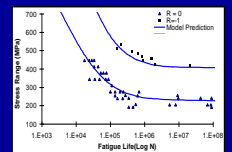
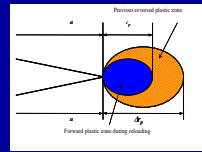
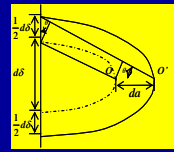


- **Physics-based probabilistic fatigue damage prognosis methodology**
  - Existing models are not suitable for concurrent prognosis and diagnosis analysis
- **Comprehensive uncertainty management framework for prognostic algorithms**
  - A comprehensive uncertainty quantification, propagation and updating scheme is lacking for prognostic algorithms
- **Rigorous model verification and validation methodology and its associated metrics**
  - No available prognosis metrics for time-dependent RUL prediction
- **Experimental testing to demonstrate, validate, and compare fatigue damage prognostic algorithms**
  - Multi-level experimental study for hypotheses verification, prediction validation, and application demonstration

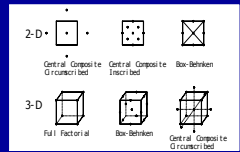
# Validation and uncertainty management of prognostic algorithms



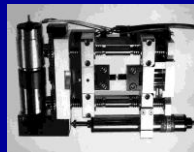
Fatigue crack growth modeling



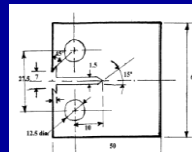
Life prediction methodology



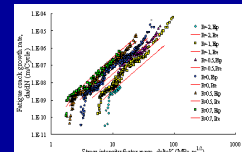
Design of Experiments



In-situ fatigue testing



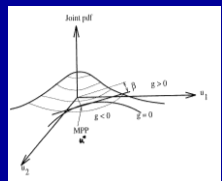
Long crack testing



Crack growth measurements

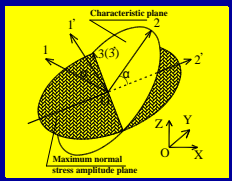
**Probabilistic Fatigue Prognosis**

**Experimental testing**

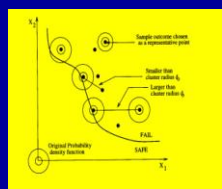


First-order reliability method

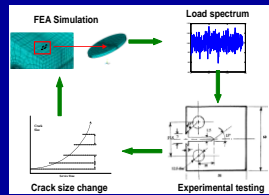
- Small and long crack growth
- Multi-axial fatigue modeling
- Life prediction methodology
- Analytical and simulation methods



Multi-axial fatigue analysis

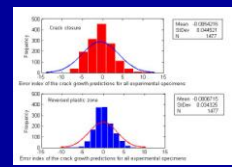


Adaptive importance sampling

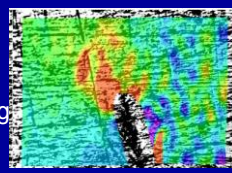


Hybrid simulation/experimental testing

- Design of Experiments
- Uniaxial fatigue testing
- Multiaxial fatigue testing
- Hybrid simulation/experimental testing

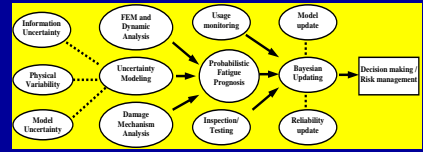


Data analysis

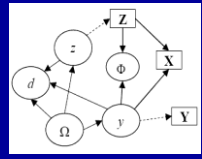


Crack growth pattern and imaging analysis

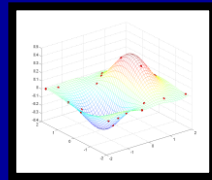
- Random process theory
- Bayesian updating
- Usage monitoring and sensors
- Non-destructive inspection



Uncertainty quantification and propagation



Bayes network

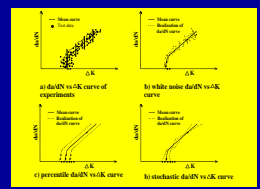


Surrogate modeling

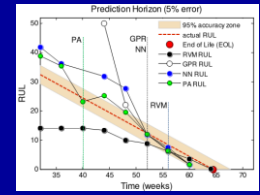
- Model error quantification
- Calibration under uncertainty
- Surrogate modeling
- Validation metrics and criteria

**Uncertainty Management**

**Model Validation**



Stochastic crack growth rate curve



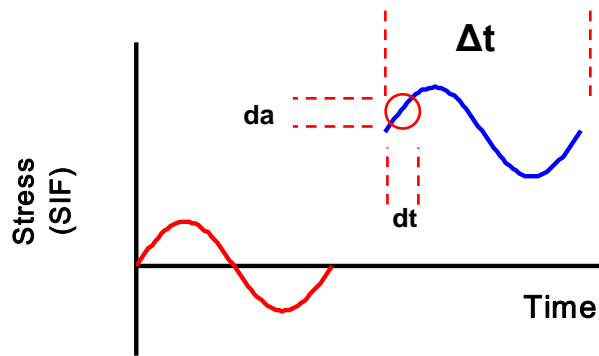
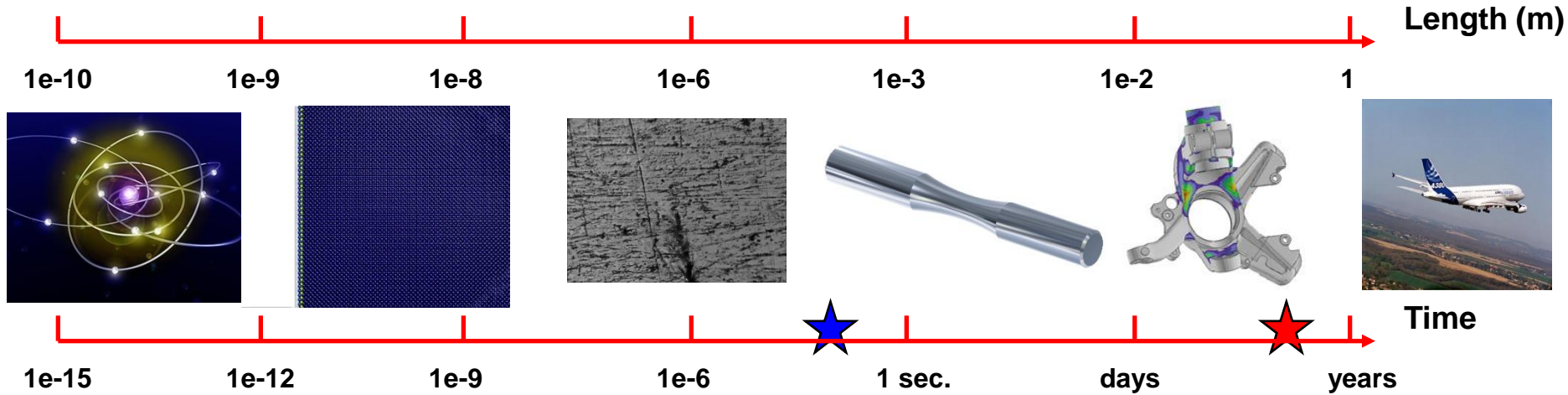
Validation metrics and criteria

# IVHM milestones being worked

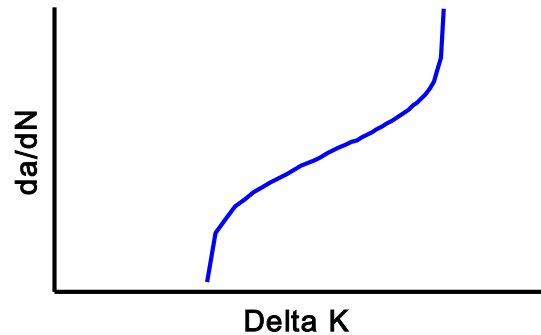
- **IVHM 3.3.2**
  - Guidelines for fidelity of prognostic estimates, "...describes the appropriate level of fidelity for physics-based models for prognostics on subsystems and components."
- **IVHM 3.3.3**
  - Methodology for assessing the performance of prognostic algorithms and methods, "...describes a rigorous statistical methodology for assessing the quality of prognostic algorithms."
- **IVHM 3.3.5**
  - Assessment of the ability to perform prognostic reasoning for at least four of the adverse events listed in Table 2 (as specified in the RTIP) with performance improvements ...
- **IVHM 1.2.3.7**
  - "Validated methodologies for prognostics uncertainty management and representation... shrink the uncertainty bounds of prediction of damage progression by 50% as measured from the initial prediction to the end of life".

This is a three year award and currently starting year 2.

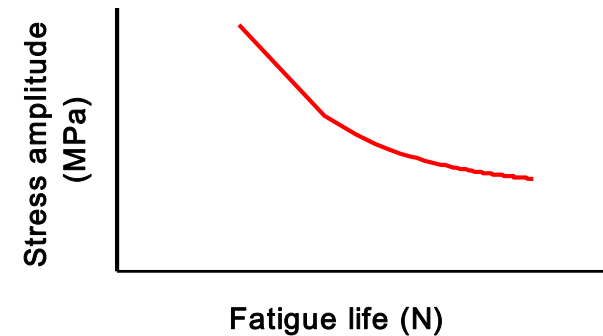
# A multi-scale approach for structural fatigue damage prognosis



da/dt relationship  
at a smaller time  
scale



da/dN curve –  
Paris, 1960's



SN curve –  
Wholer, 1860's

# Model development

Geometric relation  $da = \frac{ctg\theta}{2} d\delta = Cd\delta$  (1)

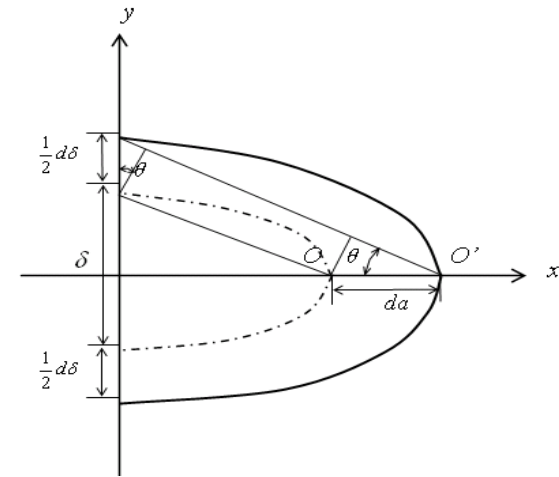
Crack Tip Opening Displacement  $\delta = \frac{4K^2}{\pi E \sigma_y} = \lambda \sigma^2 a$  ( $\lambda = \frac{4}{E \sigma_y}$ ) (2)

Instantaneous crack growth rate

$$\frac{1}{C\lambda a} \frac{da}{dt} = \frac{2\sigma}{1 - C\lambda\sigma^2} \frac{d\sigma}{dt} \quad (3)$$

General formulation of the model

$$\dot{a} = H(\dot{\sigma}) \cdot H(\sigma - \sigma_{ref}) \cdot \frac{2C\lambda}{1 - C\lambda\sigma^2} \cdot \dot{\sigma} \cdot a \quad (4)$$

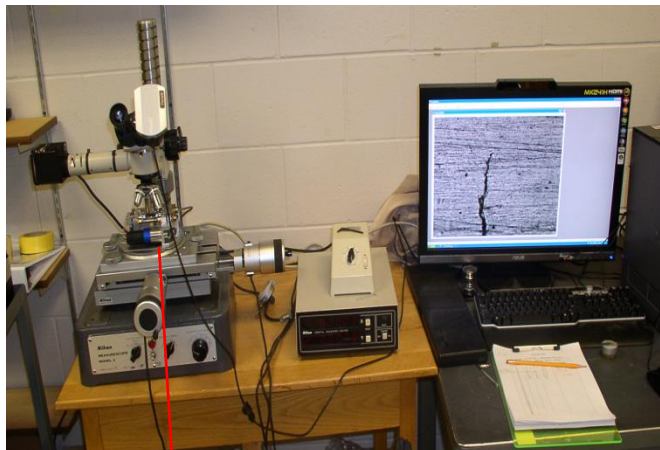


Schematic representation of crack tip geometry

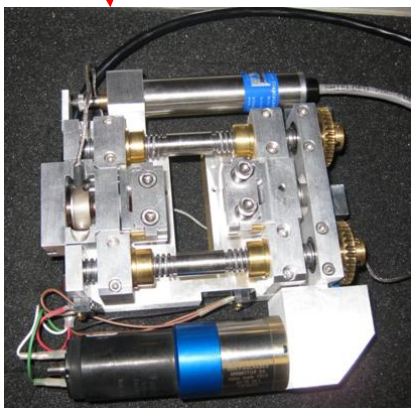
**Hypotheses 1:** crack growth is controlled by the interaction of forward and reversed plastic zone, which are influenced by crack closure

**Hypotheses 2:** crack growth is not uniformly distributed within one cycle and remains constant during majority of the loading history

# In-situ fatigue testing under optical microscope and in SEM



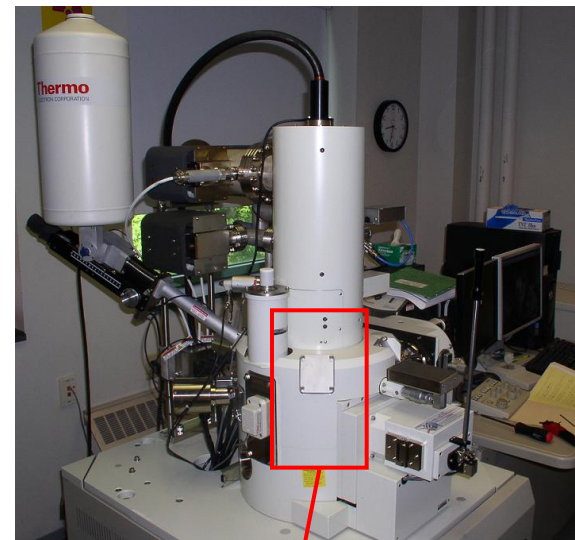
Nikon metallurgical microscope



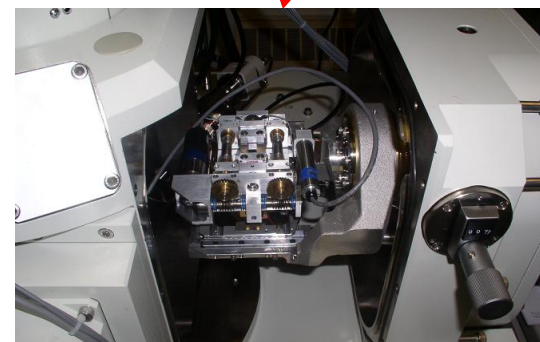
**In-situ optical microscope fatigue testing**



Controller and PC



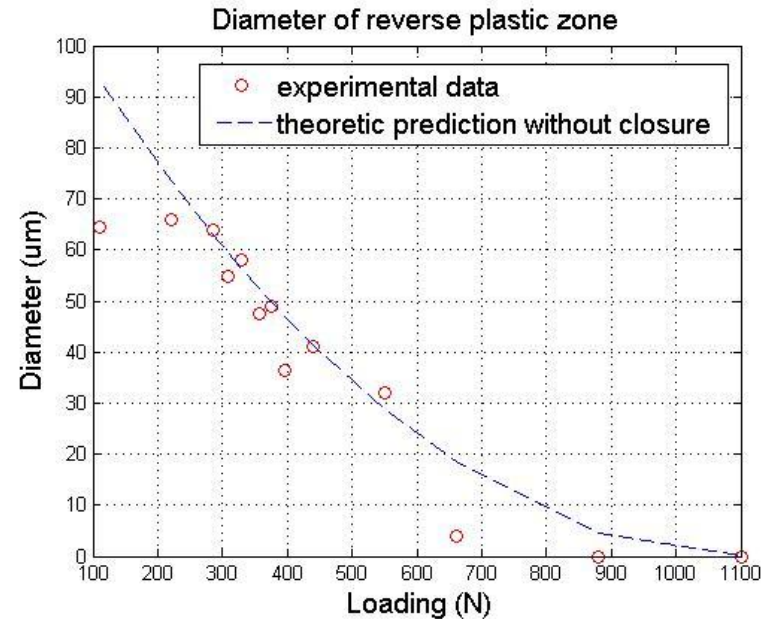
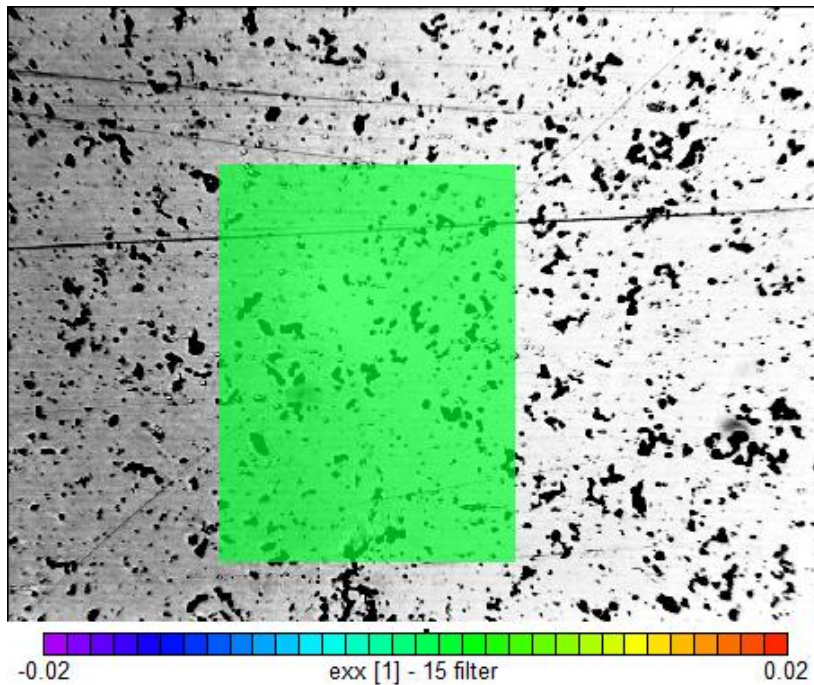
Jeol 7400-F SEM



**In-situ SEM fatigue testing**

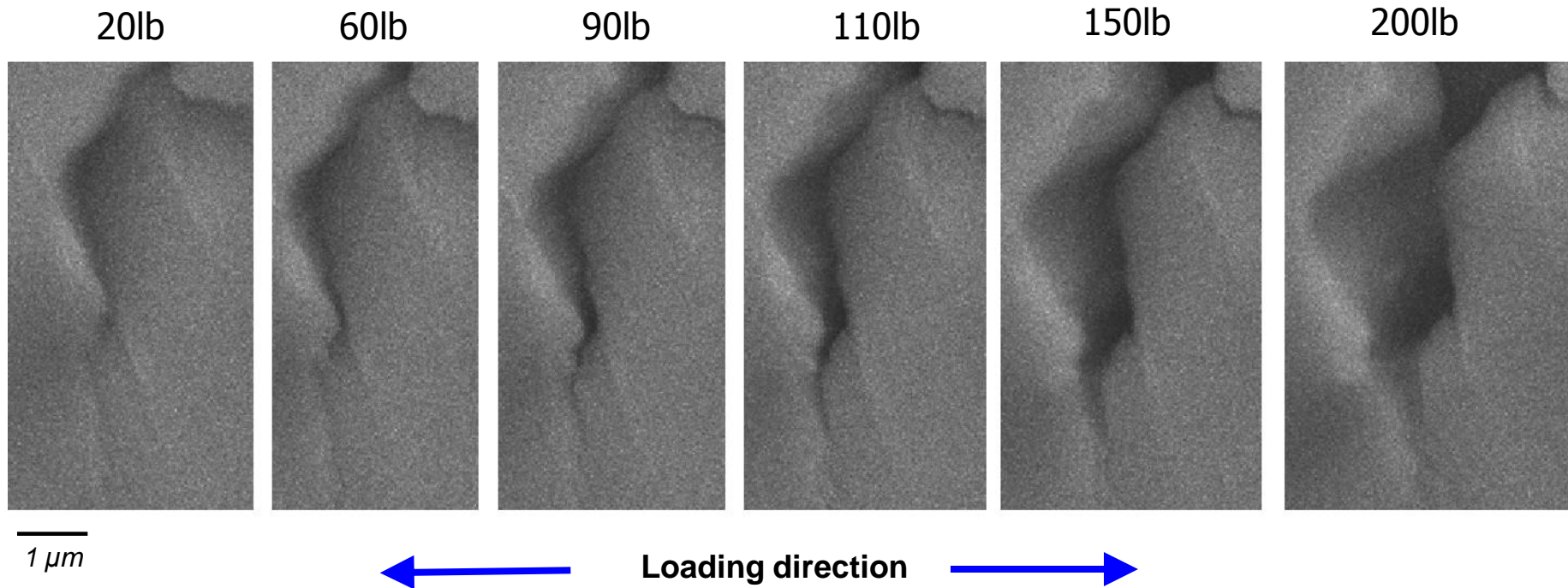


# Forward and reversed plastic zone measurement



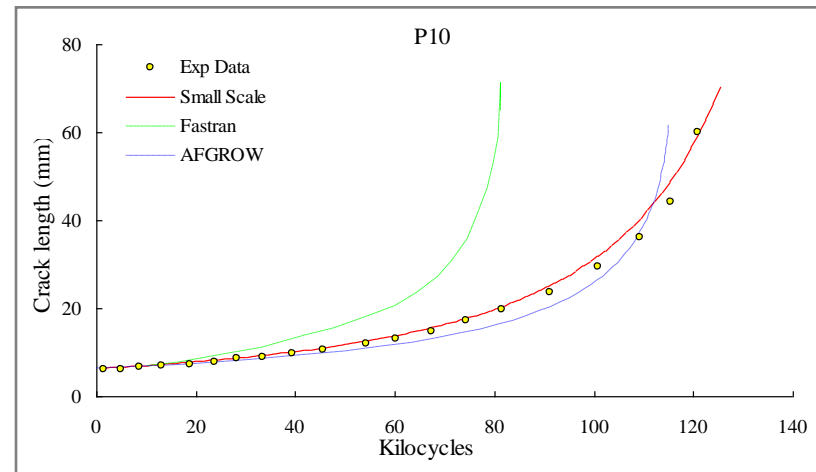
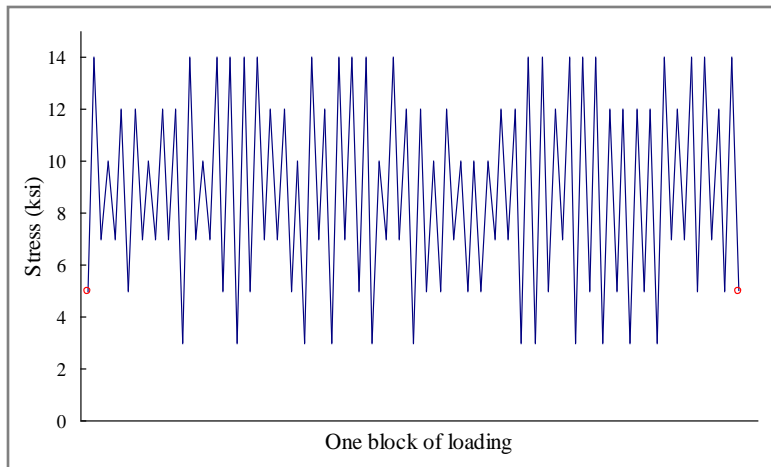
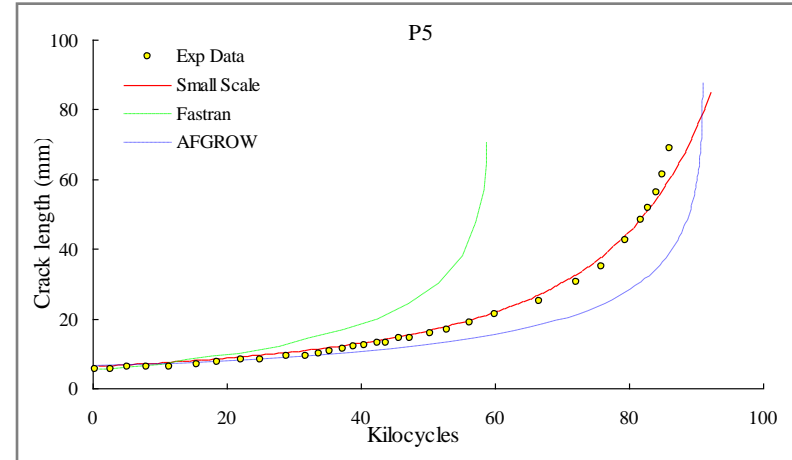
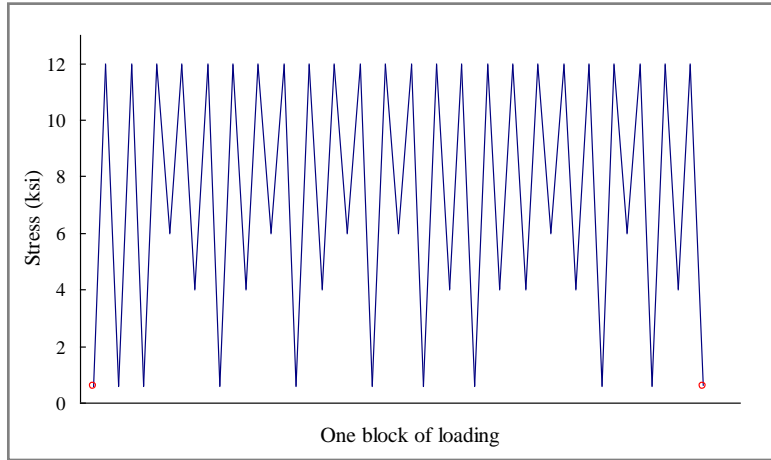
- In-situ optical microscope testing is used to measure the plastic zone size within one loading cycle
- Image correlation technique is used to estimate the crack tip strain field
- Crack closure hypothesis is verified for Al-7075-T6
- Ongoing work to include the crack blunting mechanism

# High resolution crack tip deformation and growth observation



- Both crack deformation and growth can be observed
- Crack only grows during part of the loading path and not in the unloading path
- Ongoing work focuses on the imaging analysis (registration and mapping) and additional testing under different crack growth rates

# Comparison with experimental data for model prediction



# State-space model for concurrent structural-material fatigue prognosis

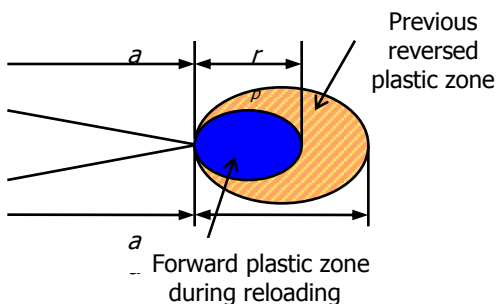
- Coupled hierarchical state-space model

Structural dynamics

$$m \ddot{x} + n \dot{x} + kx = f(t)$$

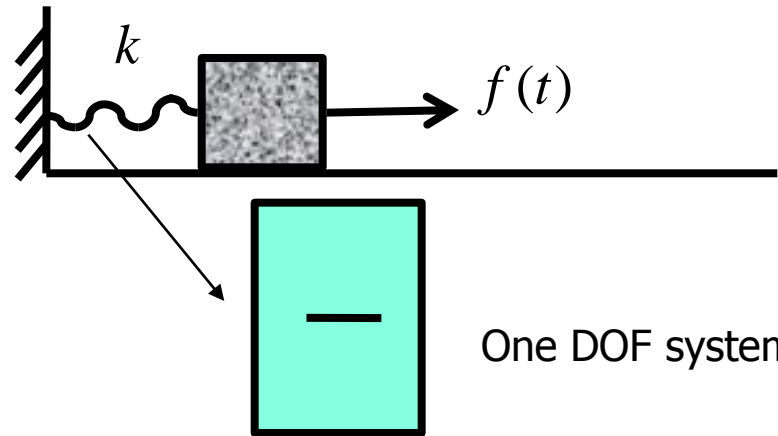
Fatigue crack growth

$$\dot{a} = H(\dot{\sigma}) H(\sigma - \sigma_{ref}) \frac{2C\lambda}{1 - C\lambda\sigma^2} \dot{\sigma} a$$

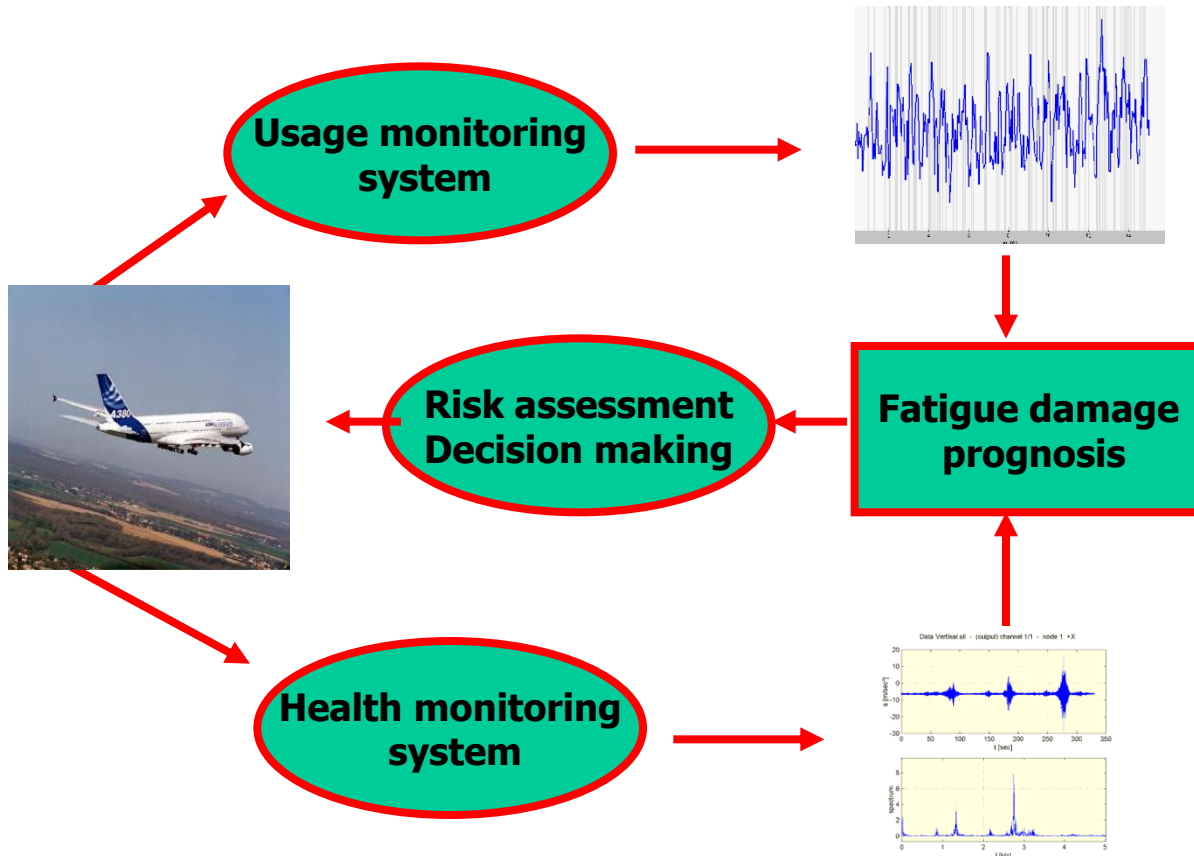
$$H(x) = \begin{cases} 1, & \text{if } x > 0 \\ 0, & \text{if } x \leq 0 \end{cases}$$



$$\begin{cases} \dot{x}_1 = x_2 \\ \dot{x}_2 = (-k(x_3)/m)x_1 + (-n/m)x_2 + f(t)/m \\ \dot{x}_3 = H(g(x_2))H(g(x_1) - \sigma_{ref}) \frac{2C\lambda}{1 - C\lambda g(x_1)^2} g(x_2)x_3 \end{cases}$$

$$y = q(x_1, x_3)$$



# Structural damage prognosis integrating health and usage monitoring systems



**Structural dynamics**

$$\begin{bmatrix} \dot{y} \\ y \end{bmatrix}_{2N \times 1} = \begin{bmatrix} [0]_{N \times N} & [I]_{N \times N} \\ [K]_{N \times N} & [C]_{N \times N} \end{bmatrix} [y]$$

$$\sigma = E(y, \dot{y} \dots)$$

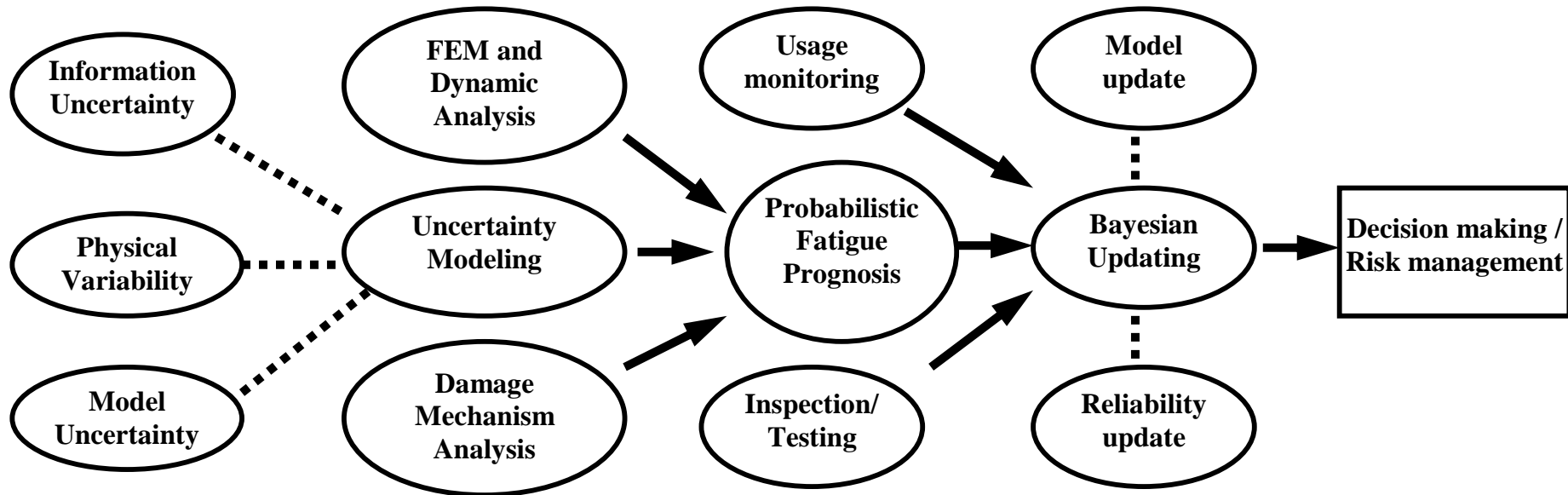
**Incremental crack growth model**

$$\dot{a} = f(\sigma, \dot{\sigma}, x_i)$$

**Healthy state features**

$$H = g(\sigma, \dot{\sigma}, a, K, C, \dots)$$

# Framework of the proposed uncertainty management methodology



- A sound uncertainty management methodology
  - Uncertainty Quantification (UQ)
  - Uncertainty Propagation (UP)
  - Uncertainty Updating (UU)
  - Risk Assessment (RA)

- Physical variability
  - Loading (multi-axial variable amplitude)
  - Material Properties
- Data uncertainty
  - Sparseness of data available to quantify material property statistics
  - Measurement uncertainty (final crack size)
- Model uncertainty/errors
  - Finite element discretization error (Richardson extrapolation)
  - Gaussian process surrogate model prediction
  - Coefficients of selected crack growth model
  - Model form error terms
- Uncertainty in inspection
  - Crack detected → Use crack size and measurement error in inference
  - No crack detected → use POD (Probability of detection) in inference

Basic idea: model the output  $Y$  as a Gaussian process which is indexed by the inputs  $\mathbf{x}$ .

Training: Given  $m$  training points  $\mathbf{x}_1, \dots, \mathbf{x}_m$ , with corresponding outputs  $\mathbf{Y} = [Y(\mathbf{x}_1), \dots, Y(\mathbf{x}_m)]^T$ , the joint distribution of  $Y$  is defined by

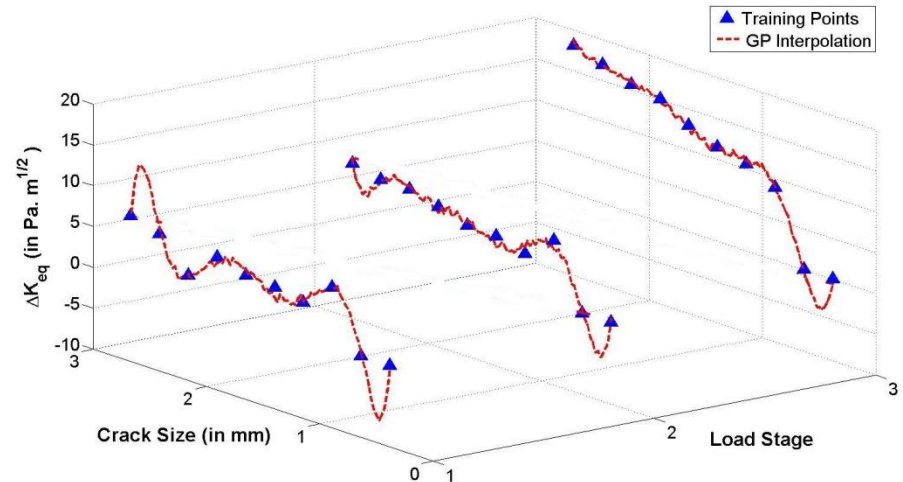
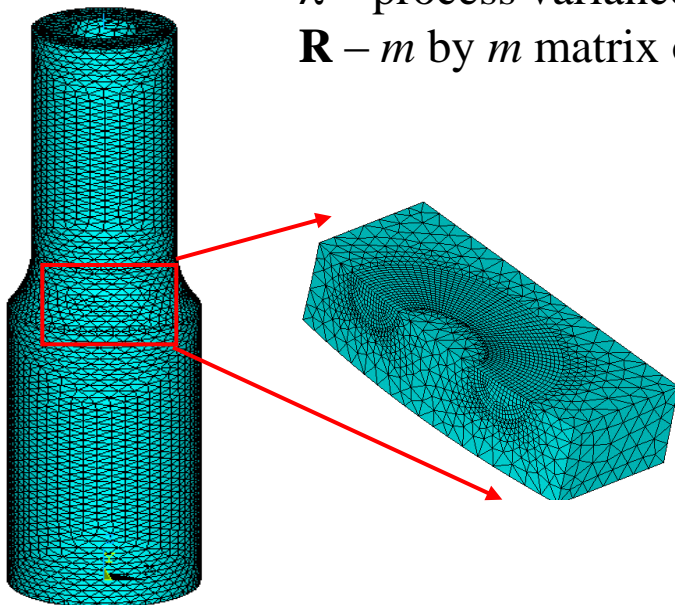
$$\mathbf{Y} \sim N_m[\mathbf{f}^T(\mathbf{x})\boldsymbol{\beta}, \lambda\mathbf{R}]$$

$\mathbf{f}^T$  –  $q$  basis functions for the trend -- linear or quadratic

$\boldsymbol{\beta}$  – coefficients of the regression trend

$\lambda$  – process variance,  $\lambda = \sigma^2$

$\mathbf{R}$  –  $m$  by  $m$  matrix of correlations among the training points





Suppose the following information is known:

limit state function (Eq. (a))

target reliability/confidence level (Eq. (b))

$$\left\{ \begin{array}{l} (a): g(x, y) = 0 \\ (b): \|x\| = \beta \end{array} \right.$$

Inverse FORM (IFORM) is to find a solution of  $y$  to satisfy the above constraints

vector  $x$  : random variables (e.g., material properties, load, structural geometries, etc.)

vector  $y$  : index variables (e.g., time, coordinates, variables with small randomness, etc.)

- No sampling required and suitable for both ground-based and on-line prognosis

- Directly calculate the RUL at a given confidence/reliability level

- Limit state function

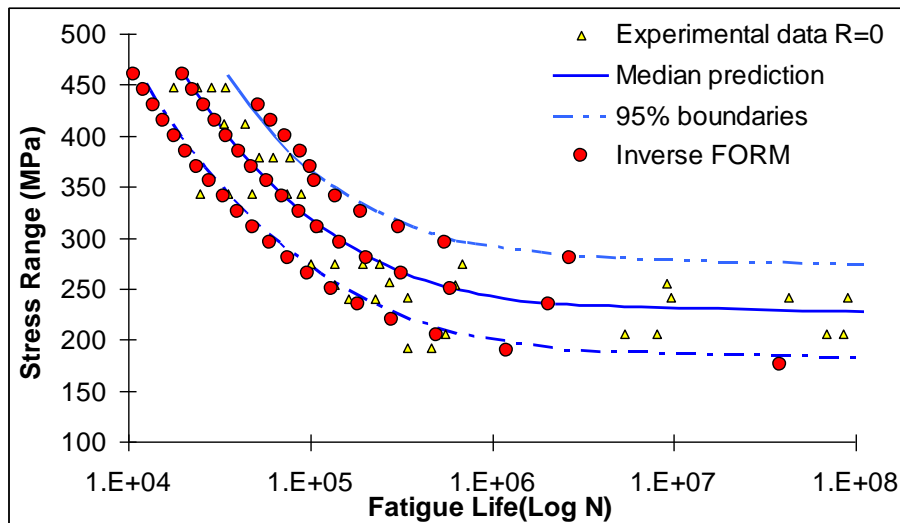
$$g(A, a_i, N) = \log \left( \int_{a_i}^{a_c} \frac{1}{Ab^R [\Delta K - \Delta K_{th}]^m} da \right) - \log(N)$$

$$\left. \begin{array}{l} \nabla_x g(x) = \begin{cases} \frac{1}{A} \\ - \frac{1}{\int_{a_i}^{a_c} \frac{1}{Ab^R [\Delta K - \Delta K_{th}]^m} da} \end{cases} \\ \frac{\partial g}{\partial N} = -\frac{1}{N} \end{array} \right\}$$

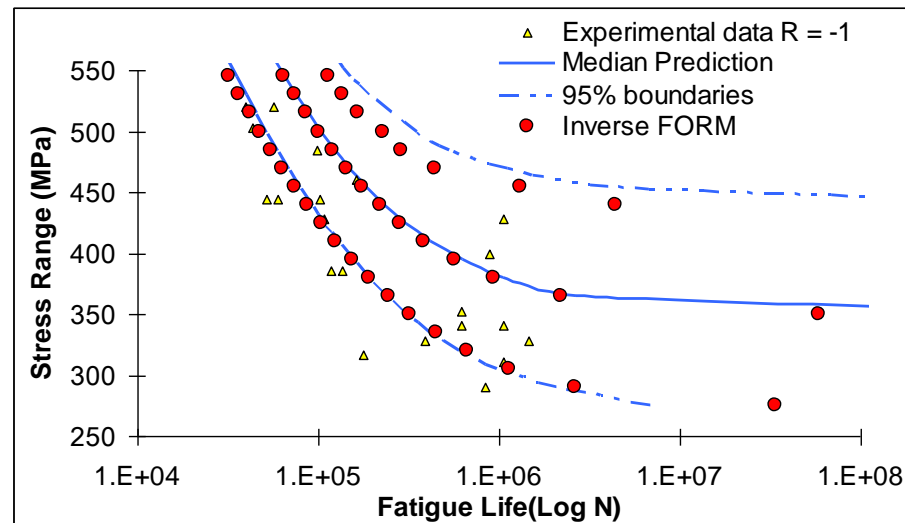
- Iterative calculation using Newton-Raphson method

$$\begin{cases} X_{k+1} \\ N_{k+1} \end{cases} = \begin{cases} X_k + a_1 \left( \frac{[\nabla_x g(x, N) \bullet x] - g(x, N)}{\|\nabla_x g(x, y)\|^2} \nabla_x g(x, N) - X_k \right) + a_2 \left( -X_k - \beta_{target} \frac{\nabla_x g(x, N)}{\|\nabla_x g(x, N)\|} \right) \\ N_k + a_2 \frac{[\nabla_x g(x, N) \bullet x] - g(x, N) + \beta_{target} \|\nabla_x g(x, N)\|}{\frac{\partial g(x, N)}{\partial N}} \end{cases}$$

# An example for probabilistic life prediction – Al 7075



R=0



R=-1

- Proposed IFORM method capture the trend and the scatter in the experimental data
- Give similar prediction accuracy compared to that of the direct Monte Carlo method
- IFORM is very efficient compared to the direct Monte Carlo method

Liu, Y., Mahadevan, S., "Probabilistic fatigue life prediction using an equivalent initial flaw size distribution", International Journal of Fatigue, Vol. 31, Issue 3, pp. 476-487, 2009.

Xiang, Y., Lu, Z., Liu, Y., "Crack growth-based fatigue life prediction using an equivalent initial flaw model. Part I: Uniaxial loading", International Journal of Fatigue, 2009. (in press)

# Maximum Relative Entropy approach for uncertainty updating

- Uncertainty updating is a critical component for the overall uncertainty management
  - Update our belief using observations of the system response and reduce prognosis scatter band
- Classical Bayesian method is widely used  $p(\theta) \propto \mu(\theta) \cdot \mu(x' | \theta)$ 
  - Difficult to handle moment data [1], e.g.  $\langle \sqrt{\theta} \rangle$

- Maximum Relative Entropy (MRE) approach seeks the posterior under the moment constraints

$$\begin{aligned} \text{maximize } I(p : \mu) &= - \int dx d\theta \cdot p(x, \theta) \log(p(x, \theta) / \mu(x, \theta)) \\ \text{under constraints } c_2 &: \int dx d\theta \cdot p(x, \theta) g(\theta) = \langle g(\theta) \rangle = G \end{aligned}$$

- Posterior from MRE approach is a generalized Bayesian solution

$$p(\theta) \propto \mu(\theta) \cdot \mu(x' | \theta) \cdot e^{\beta \cdot g(\theta)}$$

[1] A. Giffin and A. Caticha (2007). Updating probabilities with data and moments. In K. Knuth (Ed.), Bayesian Inference and Maximum Entropy Methods in Science and Engineering, AIP Conference Proceedings, 954:74

# Rigorous model verification and validation using prognosis metrics

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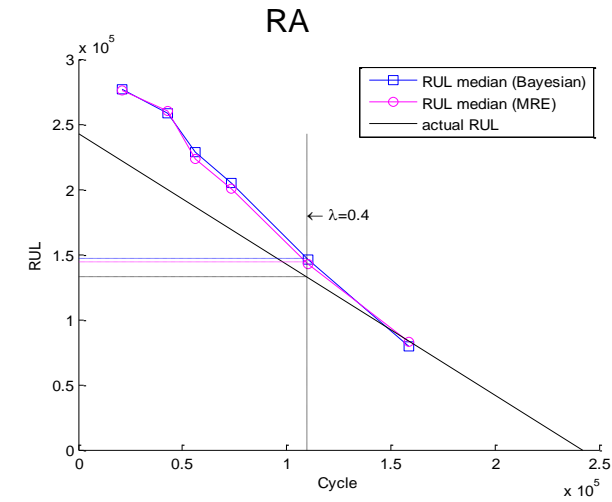
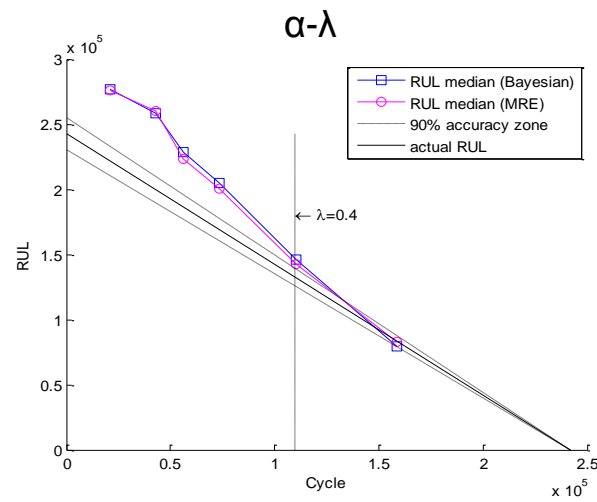
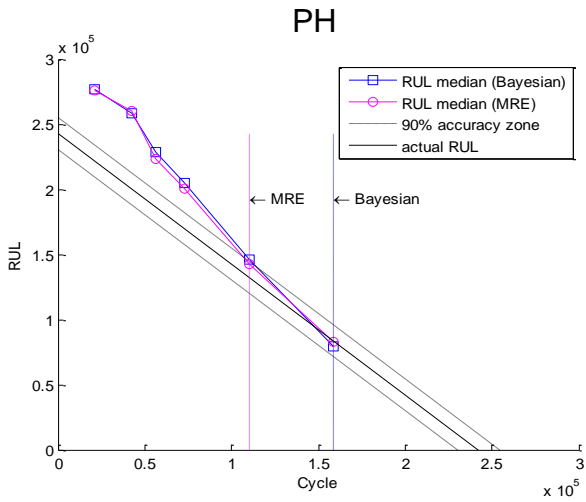
- Visual graphical comparison is useful but does not provide quantitative judgment of the investigated prognostic algorithms
- Classical metrics
  - Based on statistical analysis, a large number of samples are required
  - Difficult to describe the prognosis performance over time
- Prognostics-based metrics [1]
  - Designed to describe how well an algorithm improve over time
  - Not based on statistics, no sample required
  - 4 metrics: Prognostic Horizon (PH),  $\alpha$ - $\lambda$  accuracy, Relative Accuracy (RA), Convergence
- Demonstration using experimental testing data [2-3]
  - Experimental data: AI 2024-T3 in Virkler's and McMaster's dataset
  - Physics model: fatigue crack growth analysis
  - Probabilistic prognosis: MRE and Bayesian

[1] A. Saxena, J. Celaya, B. Saha, S. Saha, and K. Goebel (2009). Evaluating algorithm performance metrics tailored for prognostics. IEEE Aerospace conference, 7-14 March 2009, pp. 1-13.

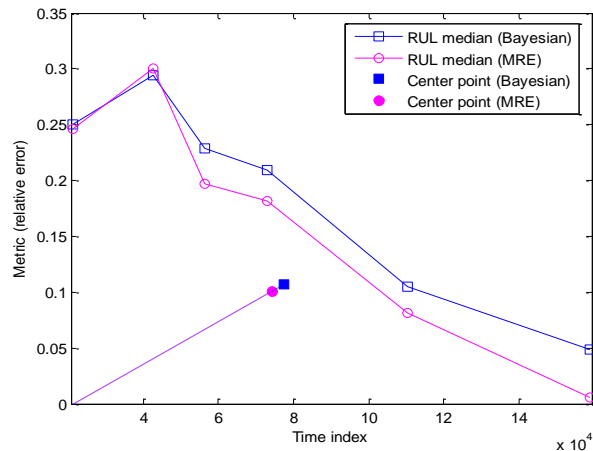
[2] Guan, X., Jha, R., **Liu, Y.**, "Probabilistic fatigue damage prognosis using maximum entropy approach", Journal of Intelligent Manufacturing, 2009. (accepted)

[3] Guan, X., **Liu, Y.**, Saxena, A., Celaya, J., Goebel, K., "Entropy-based probabilistic fatigue damage prognosis and algorithmic performance comparison", annual conference of the prognostics and health management society, San Diego, CA, 2009.

# Prognosis metrics – Virkler’s dataset

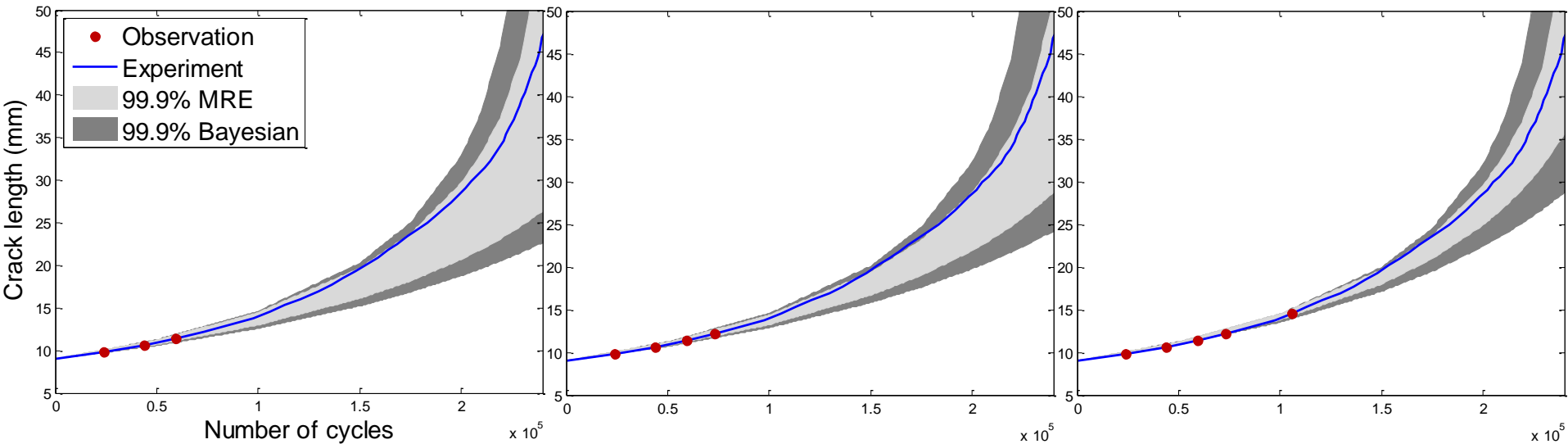


## Convergence



Metric	MRE	Bayesian
MAPE	8.66	10.93
Average Bias (cycles)	10956.27	14051.92
STD(cycles)	7628.77	9115.78
MSE(cycle <sup>2</sup> )	178.23 $\times 10^6$	280.5 $\times 10^6$
PH <sub><math>\alpha=10\%</math></sub>	183283	169451
RA <sub><math>\lambda=0.4</math></sub>	0.92	0.89
CRA <sub><math>\lambda=0.4</math></sub>	0.89	0.87
Convergence (RA)	74365.72	77349.24

# Prognosis confidence bounds estimation (Virkler's dataset)



- Both MRE and Bayesian can narrow down the confidence bounds using additional observations
- Similar conclusions can be seen from the McMaster's data
- Differences between MRE and Bayesian are case dependent, especially on the choice of prior distribution during the updating process
- Additional theoretical and experimental work are ongoing for new validation and new metrics development

# Conclusions

- A general physics-based probabilistic fatigue damage prognosis methodology has been developed
- Novel small time scale fatigue formulation for concurrent multiscale fatigue damage modeling
- Comprehensive uncertainty quantification framework including various modeling and measurement errors
- Advanced surrogate modeling based on Gaussian Process (GP)
- Efficient probabilistic life prediction method for both ground-based and on-line prognosis
- Maximum Relative Entropy (MRE)/Bayesian updating to shrink the confidence bounds in the life prediction
- Rigorous prognostics-based metrics for quantitative algorithm performance evaluation
- Advanced in-situ optical and SEM testing for hypotheses validation



# Next Steps

- Extend the developed fatigue modeling to general multiaxial random loading
- Develop a general computational methodology for the structural level fatigue prognosis based on the developed material model
- Develop new validation metrics for probabilistic prognostic algorithm comparison
- Global sensitivity analysis to investigate the effect of different uncertainty sources on prognosis
- Develop a general methodology to handle the uncertainty from unknown future loading and investigate its impact on the health management
- Extend the Bayesian framework for loading updating based on usage monitoring system
- Continue the experimental testing to supply validation data and support the model development