

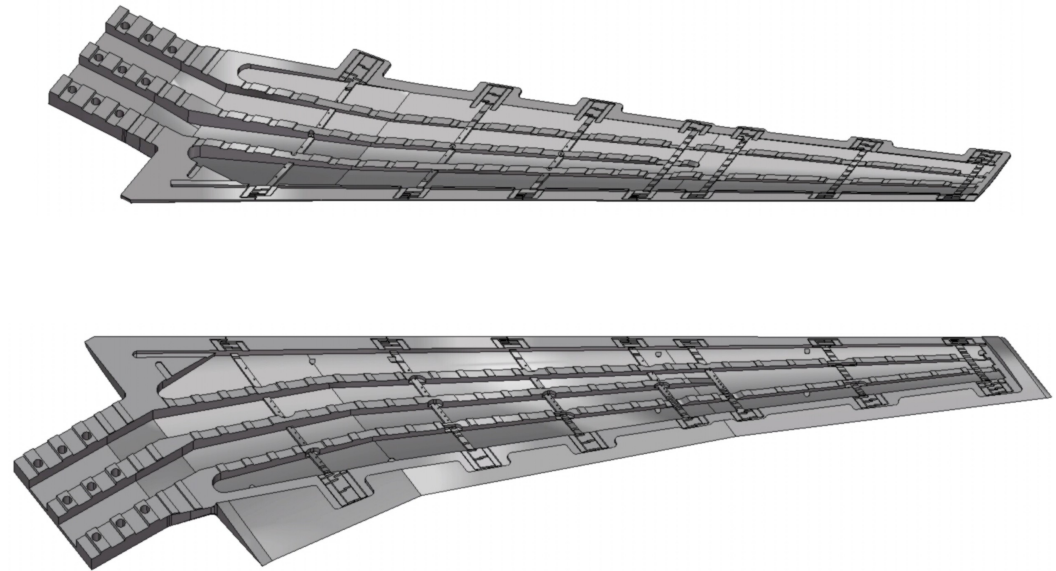
HIRENASD structural model

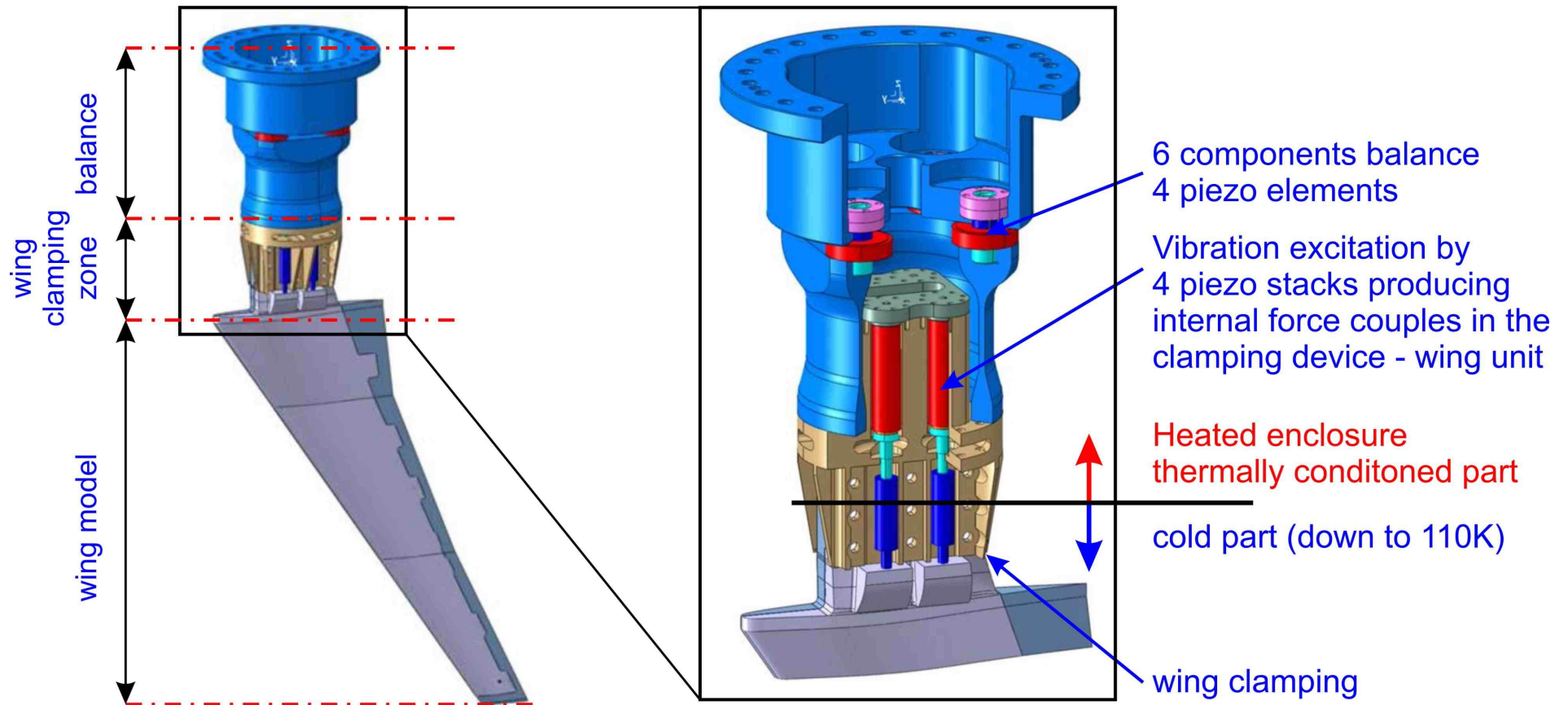
Joint exercise in Aeroelastic Prediction
RTO-203/AVT-067
Paris, 7/1/11

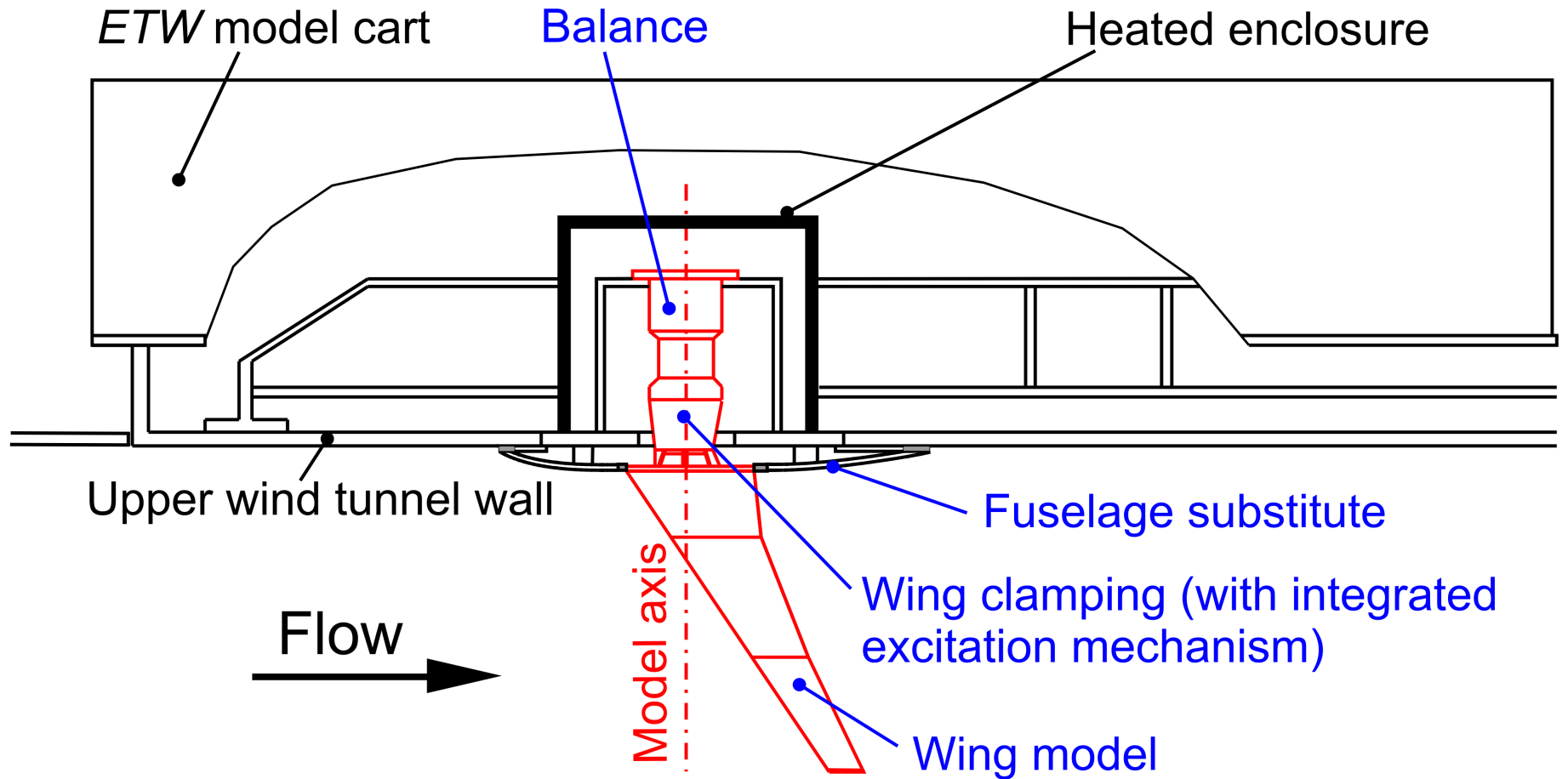
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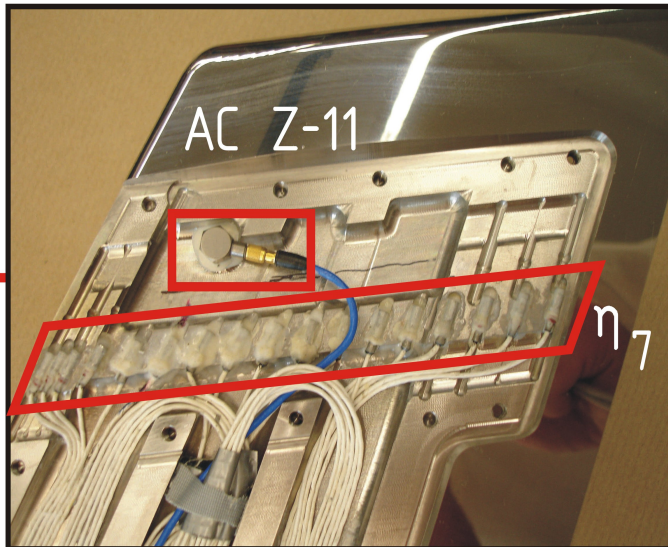
- Closer look at the structures of wing and balance
- Aims and requirements for structural modeling
- Reducing complexity: Beam model
 - Definition of beam properties and potential problems
 - Eigenmodes in comparison with measurements
 - Simulation of excitation

- Wing: Two complex shaped halves, screwed together
- Wing is exposed to temperature changes in wind tunnel
- Wing clamped to balance and filled with measuring equipment
- Complex balance, mounted in heated enclosure

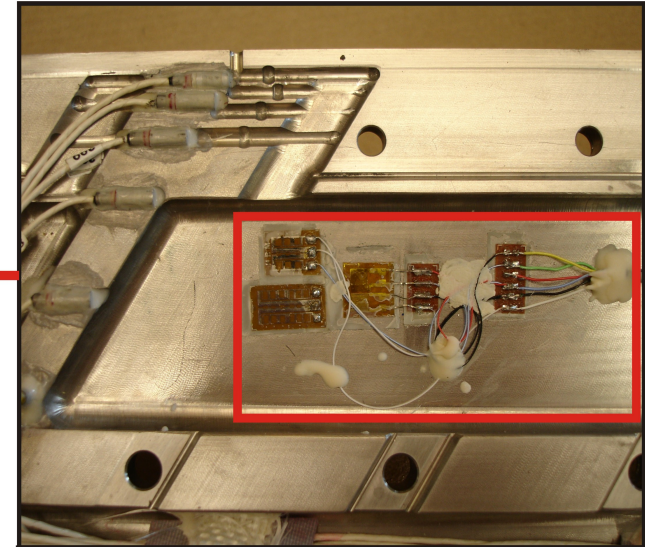




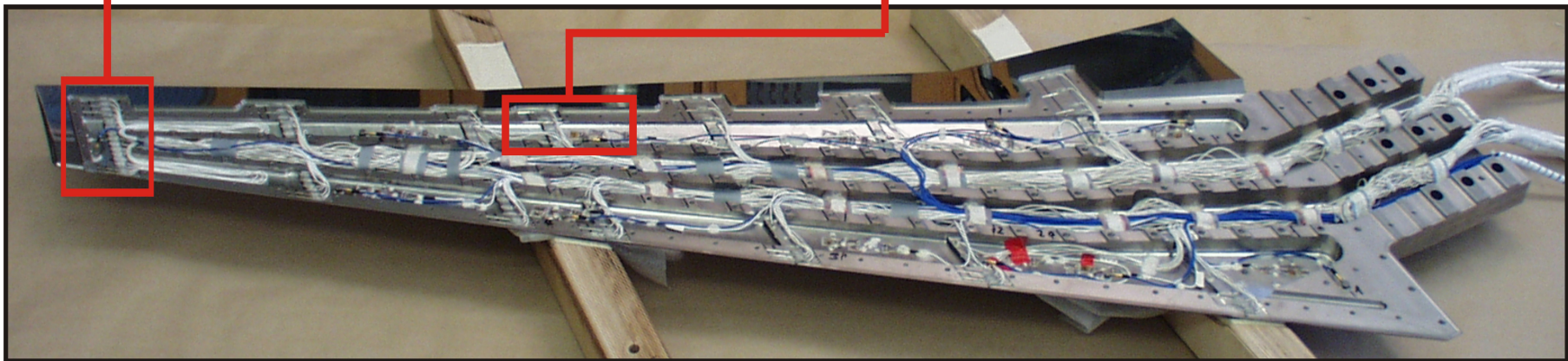




accelerometers and
in-situ pressure transducers



strain gauges



- **Aims for this project:**
 - Stationary aeroelastic solution: Correct wing deflection needed; needs fully coupled stationary solver
 - Forced excitation of mode: Can be done using
 - Forced motion of given mode shape: No need for coupled computation; needs good representation of mode shape, frequency given
 - gives unsteady aerodynamic data
 - Simulation of excitation mechanism: Needs fully coupled, non-stationary simulation; needs good representation of mode shapes and frequencies up to a certain mode
 - additional to above: aerodynamic damping
- **Not now:** Frequency shift and aeroelastic damping of modes; needs fully coupled non-stationary solver, good representation of mode shapes and reasonable frequencies.

Volume models

- “Easy” for coupling to CFD if surfaces match.

Problems for modeling:

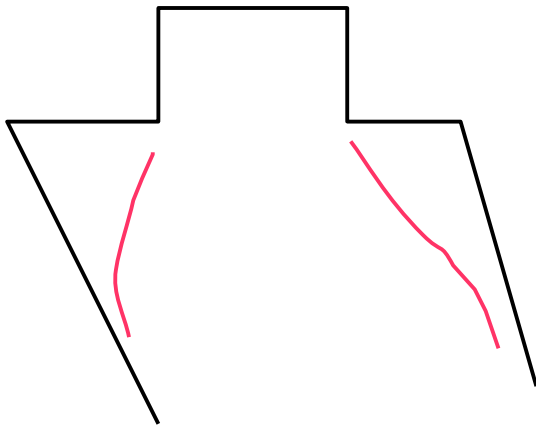
- Contact conditions between parts of wind-tunnel model
 - Equipment inside wing (extra mass)
 - If done: high computation times and possibly non-linear solver needed.
 - **Simplification:** Model of wing only as “solid” without extra mass.
- This will give good deflection results and good mode shapes for low frequencies. Frequencies will not be a good match.

Reduced order models

- Beam or shell/plate models possible. Shell models pose similar problems to full 3d modeling → Beam model
- Simplifies:
 - Much smaller equation systems
 - Represent total stiffness and mass distribution of cross section in a single value on the “axis”.
 - Quicker to adjust, so that results match with experiments
- Complication:
 - Needs matched data exchange strategy to CFD

- Define the properties of a beam section:
 - Cross section area, mass center
 - Secondary moments of inertia
 - Shear center
- For complex cross sections:
 - Exact solutions may be hard to obtain
 - Reduce complexity by using simplified cross section
 - or*
 - Use 3D-FEM simulation of long beam with this cross section to get good approximation of properties

- Problematic areas for defining beam properties:
 - Strong 3D influence (i.e. near wing root)
 - Non-unitary bodies (contact surfaces)
- Experimental data, special experiments and numerical simulation may be used to get good estimates of equivalent beam.



Eigen-Frequencies (wind off)

Beam-model vs. experiments

B=Flap bending, T=Torsion dominated

HIRENASD exp. # 304 (M=0) & 332 (M=0.75)

Beam Model F [Hz]	Mode	Experiment (120K)	
		M=0	M=0.75
25.3	1 st B	26.0	27.6
78.6	2 nd B	78.6	81.6
158.4	3 rd B	166.2	172.6
243.5	4 th B	245*	247.1
267.3	1 st T	265.8	273.1
342.1	5 th B		351.5
424.5	2 nd T		435.9

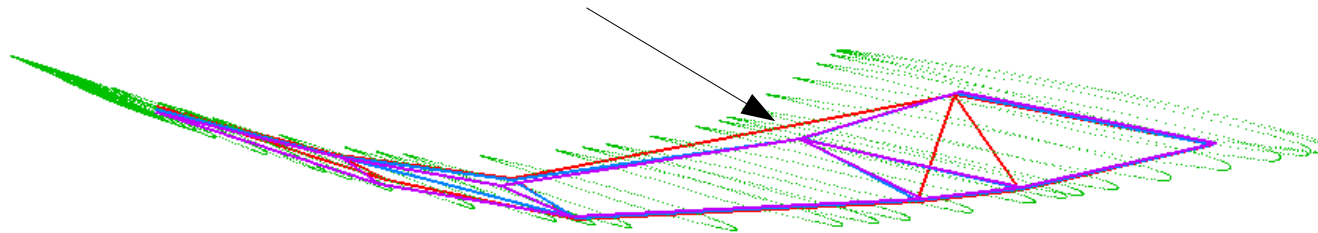
*: multiple of excitation frequency (35Hz)

1st Bending mode

25.3Hz

P304 ———
P332 ———
Beam ———

Exp. #304: Acceleration sensor broken

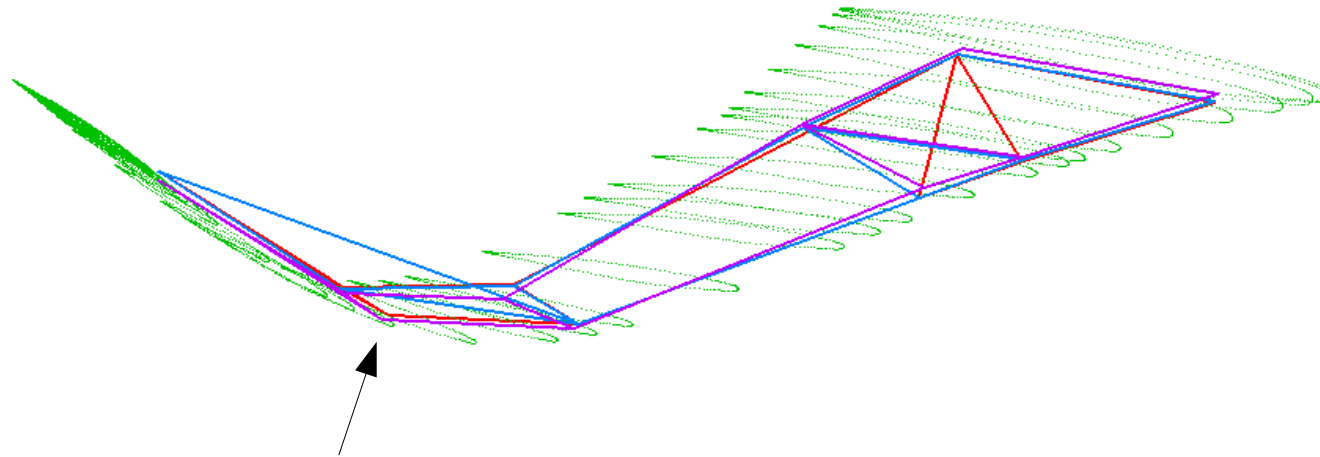


- Experiments: Mode shapes from accelerometers
#304 $M=0$; #332 $M=0.75$
- Green dots and violet shape: projection from beam model onto wing surface

2nd Bending mode

78.6Hz

P304 ———
P332 ———
Beam ———

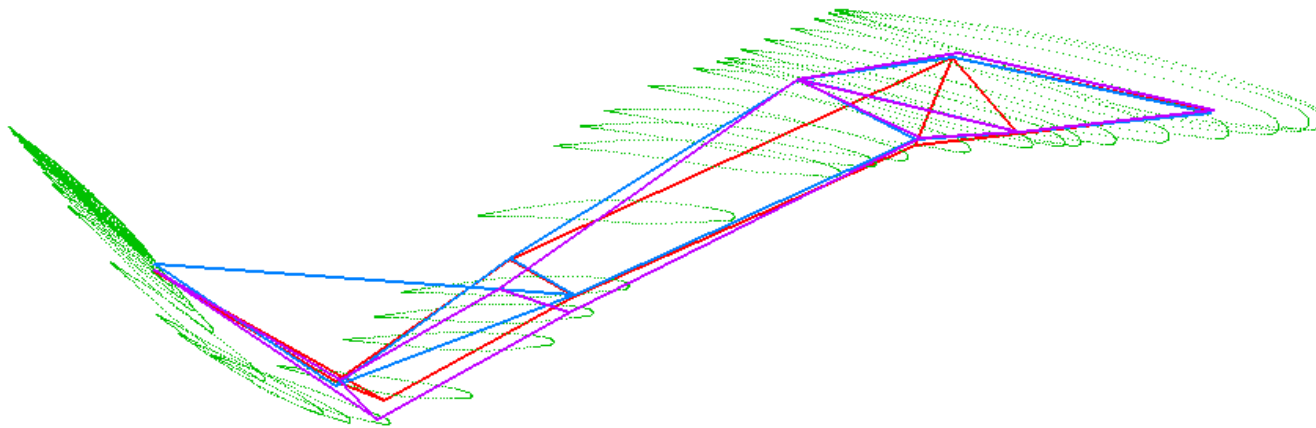


Exp. #332: Acceleration sensor broken

3rd Bending mode

158.4Hz

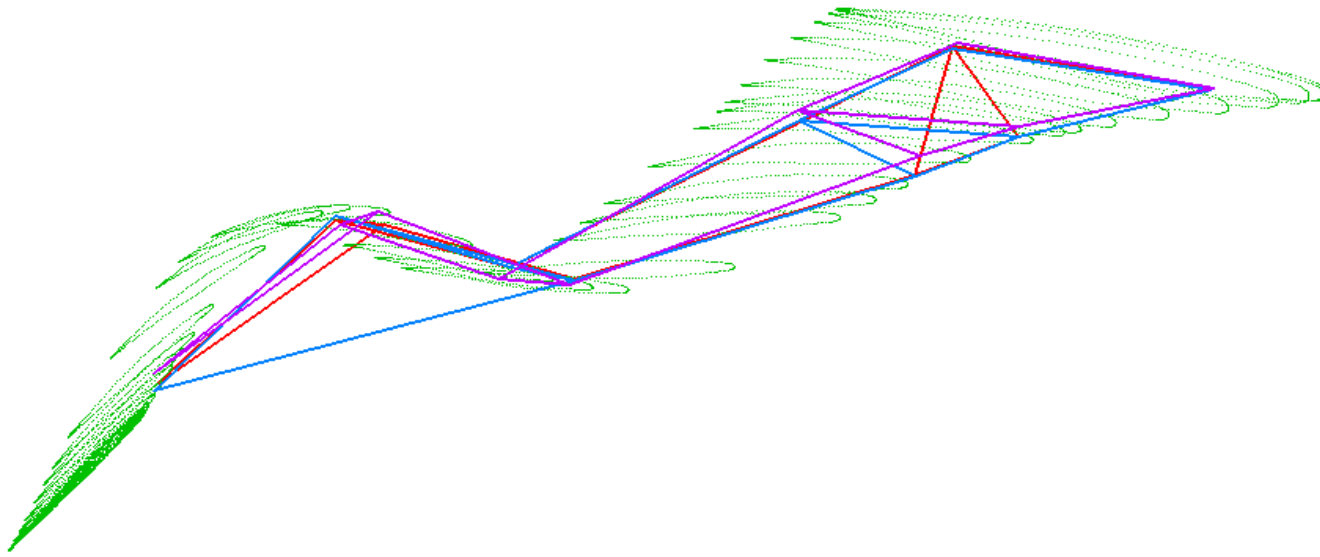
P304 ———
P332 ———
Beam ———



4th Bending mode

243.5Hz

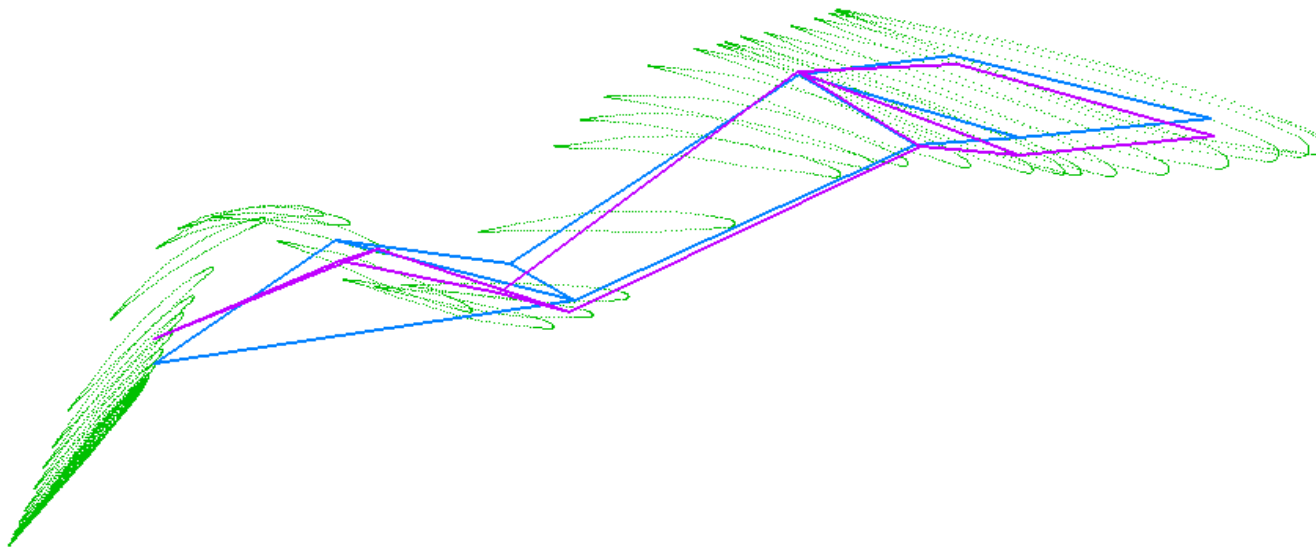
P304 ———
P332 ———
Beam ———



5th Bending mode

342.1Hz

P332 ———
Beam ———

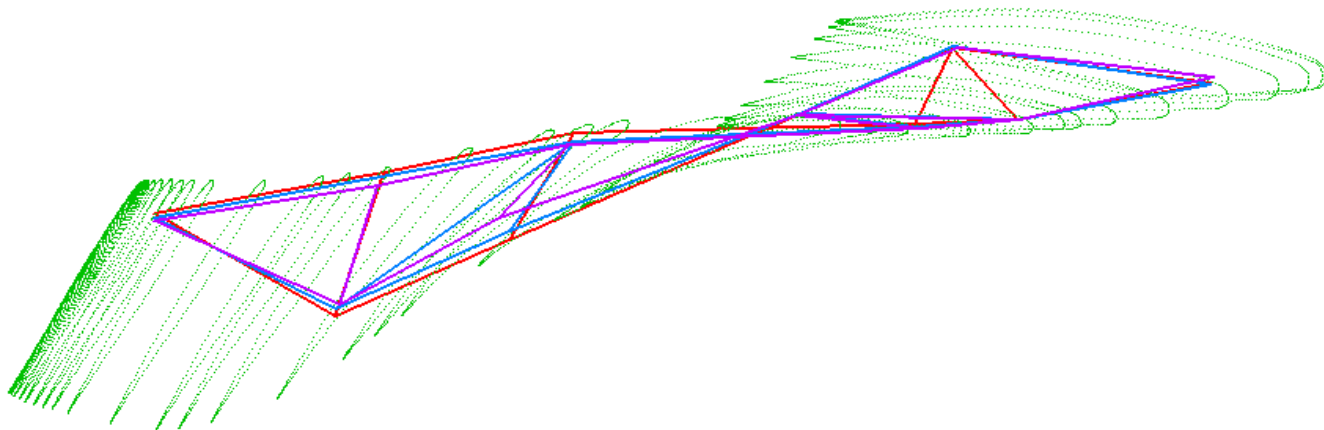


- Mode not found in wind-off trial #304
- Shapes of beam and actual wing start to diverge near wing tip

1st Torsion mode

267.3Hz

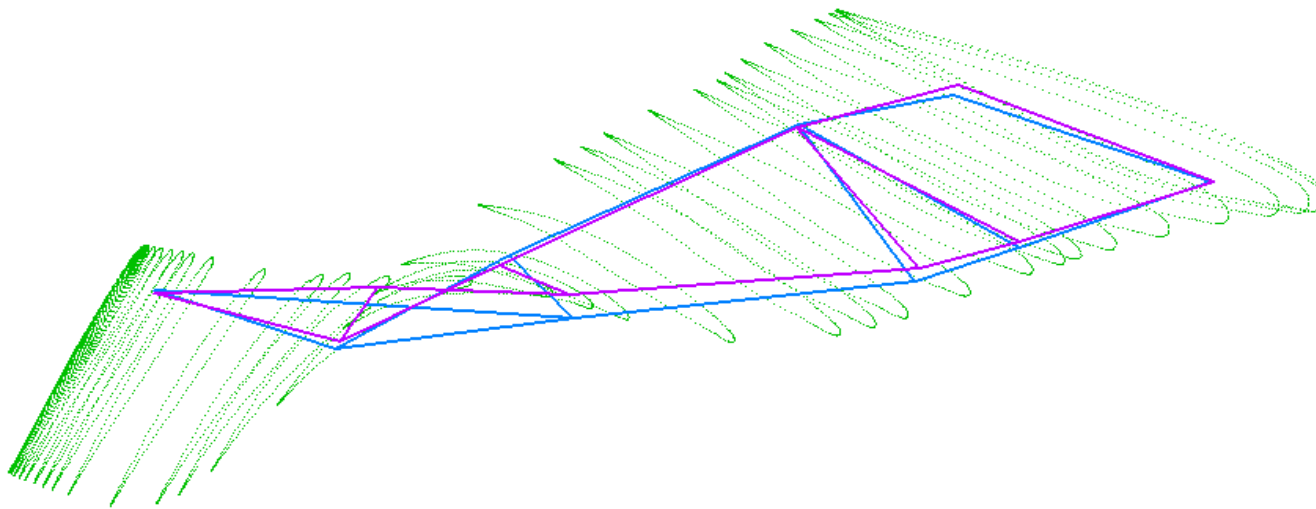
P304 ———
P332 ———
Beam ———



2nd Torsion mode

424.5Hz

P332 ———
Beam ———



Effect of wind on Eigen-frequencies

B=Flap bending, T=Torsion dominated

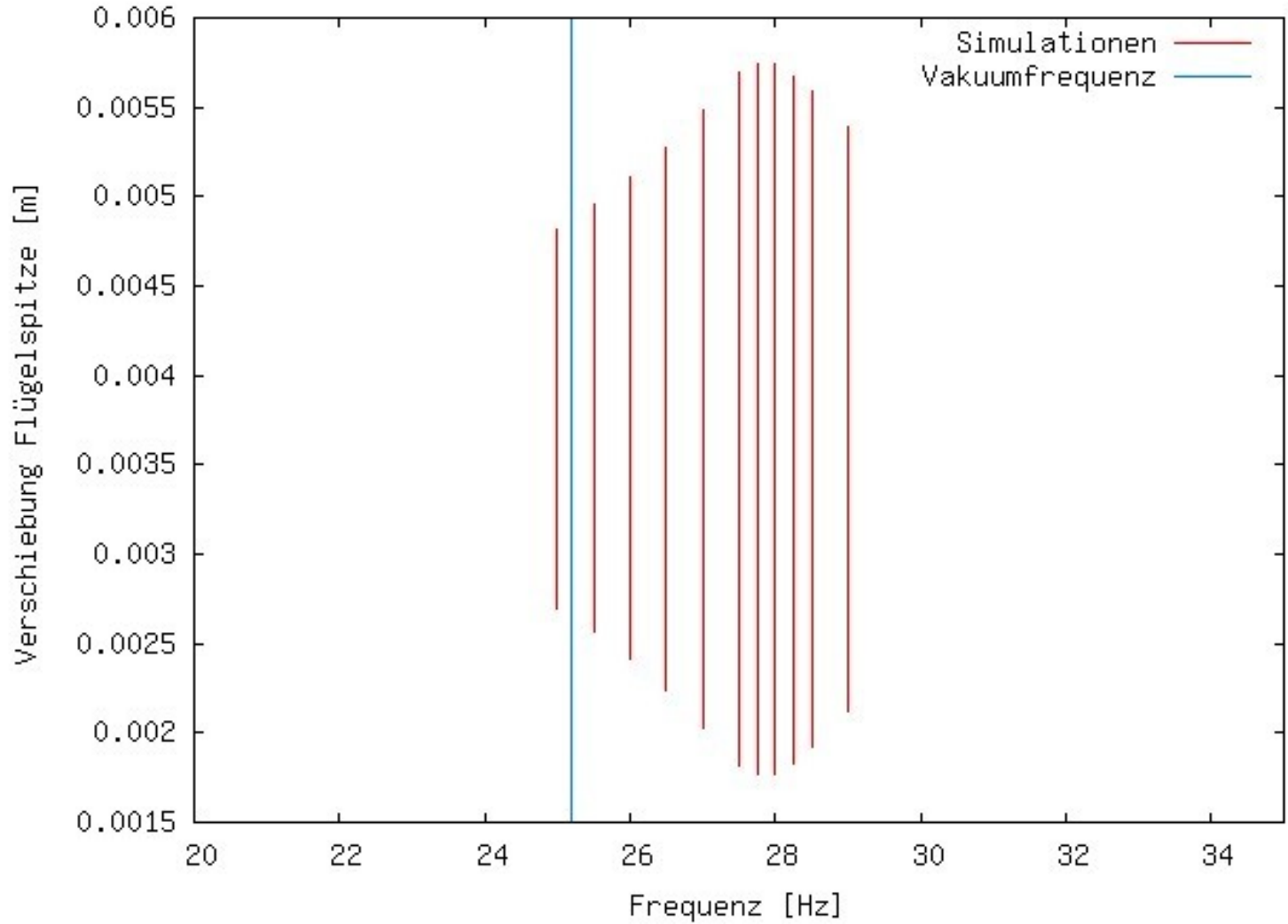
Experiments at 205K, $Re=23.5M$, $q/E=0.48E-06$

- Significant frequency shift for 1st and 2nd bending mode

Mode	M=0	M=0.7	M=0.75	M=0.8	M=0.83	M=0.85	M=0.88
1 st B	26.1	28.2	28.3	29.3	29.6	29.5	28.7
2 nd B	77.6	80.5	81	80.4	80.9	80.7	81.3
3 rd B	170	172	171.4	172.5	173	172.2	174.3
4 th B	241	243.3	242.5	242.3	242.2	242.4	243
1 st T	268	267.7	267.2	268.2	268.1	267.8	268.7

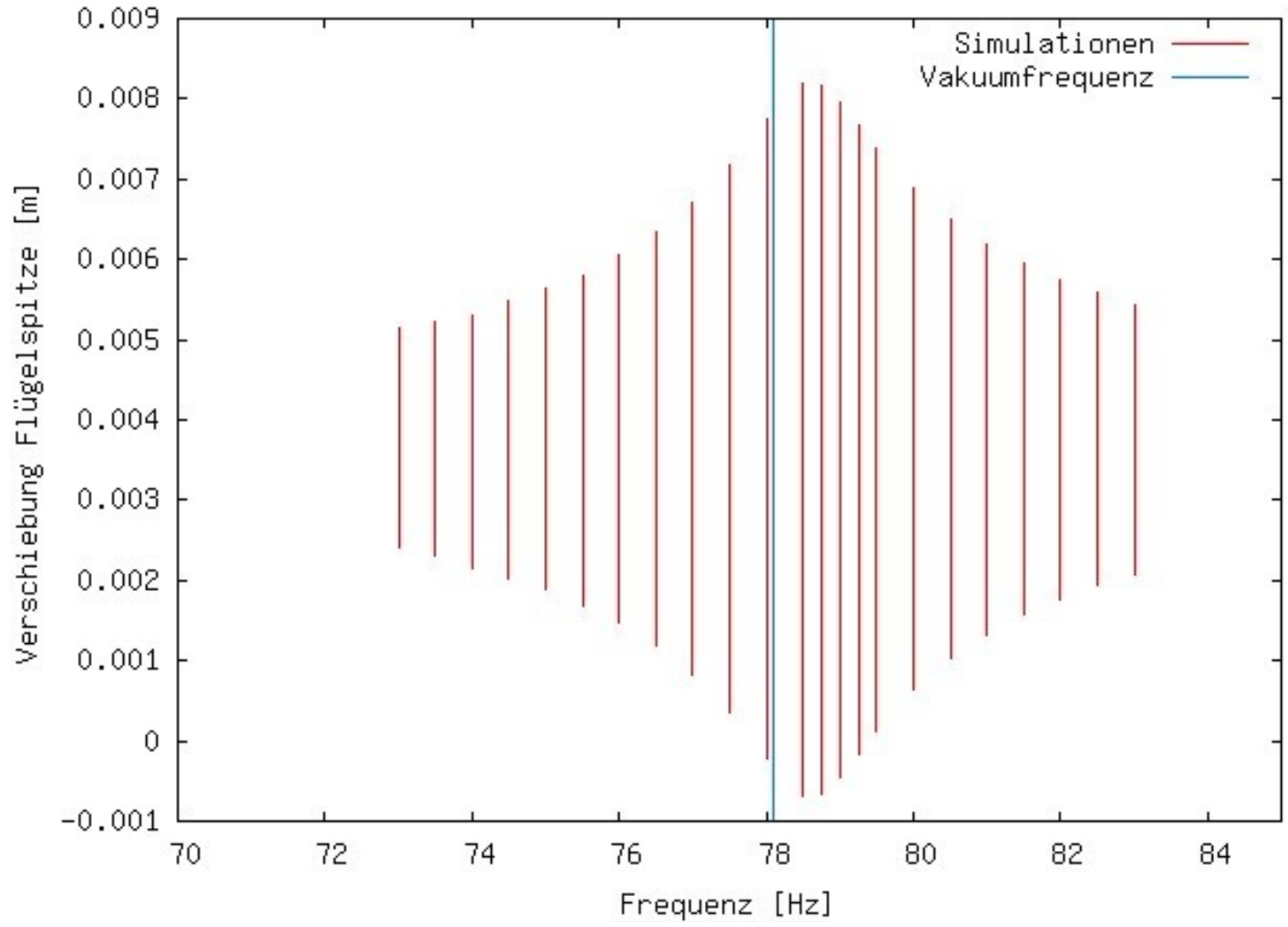
- Fully coupled simulation using reduced order model (ROM)
- Structure: beam model, but earlier stage as shown before
- Fluid: FLOWer with medium fine grid and no fuselage substitute
- Coupled simulation of forced excitation using a Volterra scheme as a ROM

1. Schlagbiegung, Simulation der Erregung, $M=0.8$, $Re=23.5\text{Mio}$, $q/E=0.48$



Frequency shift due to wind ($M=0.8$), 1st flap bending mode

2. Schlagbiegung, Simulation der Erregung, $M=0.8$, $Re=23.5\text{Mio}$, $T=205\text{K}$



Frequency shift due to wind ($M=0.8$), 2nd Flap bending mode

- Beam models allow good approximation of typical commercial aircraft wing structure
 - with good representation of
 - Mode shapes and
 - Mode frequencies
- Uncertainty in model can be addressed using comparison with experiments
- Modeling the structure for HIRENASD is a challenge of same complexity and importance as getting good CFD results