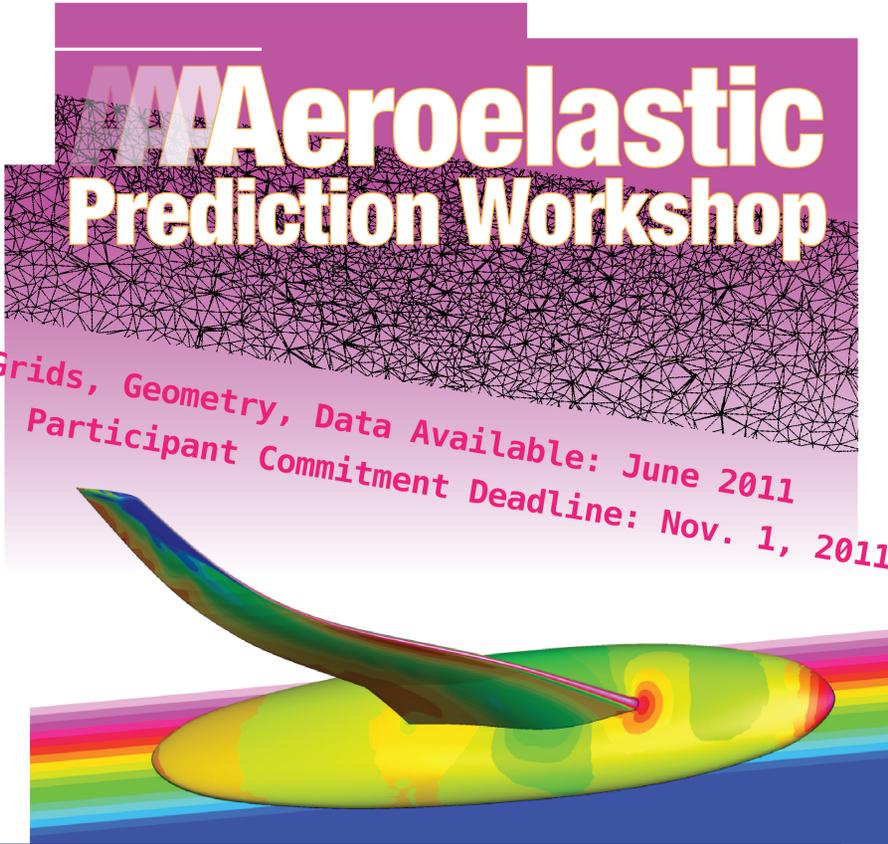


Aeroelastic Prediction Workshop:

Status Report
Presented to the
AIAA Structural Dynamics
Technical Committee

Presented
on behalf of the AePW
Organizing Committee
by
Jennifer Heeg, NASA
jennifer.heeg@nasa.gov

April 5, 2011



**AIAA Aeroelastic
Prediction Workshop**

*Grids, Geometry, Data Available: June 2011
Participant Commitment Deadline: Nov. 1, 2011*

Workshop to be held
in conjunction with

AIAA SDM Conference
Honolulu, HI
April 2012

Additional information available at:
<https://c3.ndc.nasa.gov/dashlink/projects/47/>
Or IFASD Session #18, Paris June 28, 2011

Organizing Committee Roster

Name	Affiliation	Location	E-mail	Phone
Bhatia, Kumar	Boeing Commercial Aircraft	Seattle, Washington	kumar.g.bhatia@boeing.com	
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Heeg, Jennifer	NASA	Hampton, Virginia	jennifer.heeg@nasa.gov	(757) 864-2795
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Mavriplis, Dimitri	University of Wyoming	Laramie, Wyoming	Mavripl@uwyo.edu	(307) 766-2868
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Smith, Marilyn	Georgia Institute of Technology	Atlanta, Georgia	marilyn.smith@aerospace.gatech.edu	(404) 894.3065
Whiting, Brent	Boeing Research & Technology	Seattle, Washington	brent.a.whiting@boeing.com	(206) 544-7576
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Wieseman, Carol	NASA	Hampton, Virginia	Carol.d.wieseman@nasa.gov	(757) 864-2824
Perry, Boyd	NASA	Hampton, Virginia	Boyd.perry.iii@nasa.gov	(757) 864-2840
Ballmann, Josef	Aachen University	Aachen, Germany	ballmann@itam-gmbh-de	
Taylor, Paul	Gulfstream Aerospace	Savannah, Georgia	paul.taylor@gulfstream.com	(912)965-7030

Objectives in making this presentation

- Inform TC of progress
- Address questions & concerns of SDTC, AIAA
- Ask for participation from TC members' companies, universities, agencies, ...
- Distribute sufficient information to enable participation

Objectives of AePW

Assess state-of-the-art Computational Aeroelasticity(CAe) methods as practical tools for the prediction of static and dynamic aeroelastic phenomena and responses on relevant geometries

- Perform comparative computational studies on selected test cases
- Identify errors & uncertainties in computational aeroelastic methods
- Identify gaps in existing aeroelastic databases
- Provide roadmap of path forward
 - Additional existing data sets?
 - New experimental data sets?
 - Analytical methods developments?

Guiding Principles

- Provide an impartial international forum for evaluating the effectiveness of CAe methods
- Promote balanced participation across academia, government labs, and industry
- Use common public-domain subject geometries, simple enough to permit high-fidelity computations
- Provide baseline grids and baseline structural models to encourage participation and help reduce variability of CAe results
- Openly discuss and identify areas needing additional research and development
- Conduct rigorous statistical analyses of CAe results to establish confidence levels in predictions
- Schedule open-forum sessions to further engage interaction among all interested parties
- Maintain a public-domain-accessible database of geometries, grids, and results
- Document workshop findings; disseminate this information through publications and presentations

Building block approach to validation

- Utilizing the classical considerations in aeroelasticity
 - Fluid dynamics
 - Structural dynamics
 - Fluid/structure coupling

Validation Objective of 1st Workshop

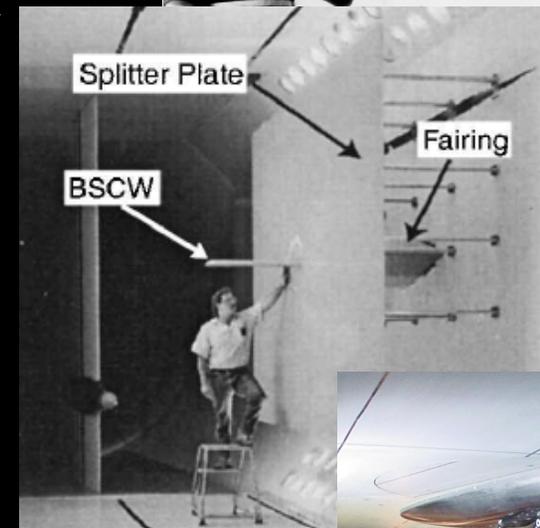
- Unsteady aerodynamic pressures due to forced modal oscillations

Future Workshops

- Directed by results of this workshop
- Directed by big-picture assessment of needs & interests

Configurations Selected

- Rectangular Supercritical Wing
 - Simple, rectangular wing
 - Static and forced oscillation pitching motion
 - Attached fully turbulent flow, moderate shock strength
- Benchmark Supercritical Wing
 - Simple, rectangular wing
 - Data acquired under mixed attached/separated flow conditions
- HiReNASD
 - 3-D aeroelastic wing with generic fuselage model
 - Steady and forced (structural resonance) oscillation testing
 - Data includes balance forces for integrated load comparisons, mean and fluctuating pressure data, and surface deformation data from optical and strain measurements during testing



Aeroelastic Prediction Workshop Schedule

- Identify organizing committee by Dec 1, 2010
- Data Release & Workshop Kickoff: IFASD, June 2011, Paris
- 9 months to perform computations
- Workshop: SDM, April 2012, Honolulu
- Perform revised computations; perform comparative analyses
- Prepare papers for formal conference presentations

Activity	FY10	FY11	FY12	FY13	FY14	FY15
Advocate	[Orange bar]					
Form organizing committee		[Black triangle]				
Workshop kick-off		[Black triangle]	Kickoff at IFASD			
Config, grids, etc. available on-line	[Yellow triangle]	[Black triangle]				
Perform analysis of selected config.			[Orange bar]			
Conduct 1 st Aeroelastic Prediction Workshop			[Black triangle]			
Update / improve CFD results / code(s)				[Orange bar]		
Perform comparisons, Statistical analyses				[Orange bar]		
Present conference papers					[Black triangle]	

AIAA AePW Liason Information

- SDTC Liason: Brent Whiting participating in AePW Organizing Committee
- AePW Liason with AIAA:
 - Jennifer Florance (NASA) coordinating with Megan Scheidt, AIAA Technical Activities Division
 - “AIAA Organized Activities at Conferences Proposal” form submitted (Proposal #11397E5)
 - Specified attendance based on High Lift PW (60 / 120)
 - Targeting weekend prior to next SDM, April 21-22,2012

AePW Website Info

- <https://c3.ndc.nasa.gov/dashlink/projects/47/>
- **Content is viewable by the world**
- **Contributions limited to members**
- **Membership by application to OC members or commitment to the workshop**

Reference Information Attached

- Publications & Briefings to be given
- Subcommittee Summaries
 - Test cases chosen
 - Gridding guidelines
 - Comparison data to be provided from computations
 - Experimental comparison data status
- Short term time line
- Configurations & Selection Rationale
- Participant Information Resources
- Overlapping activities



Reference Information Slides

Publications/Briefings

- RTO RTG 203 Telecon (March 31) J.Heeg
- AIAA/SDTC briefing at SDM (April 5) J.Heeg
- AFDC briefing (April 28-29, Huntington Beach)
K. Bhatia
- AHS Forum (May, Virginia Beach) M.Smith
- IFASD OC paper (June 28) J.Heeg
- IFASD AePW discussion panel (June 28)
 - J.Heeg, P. Chwalowski, J. Ballmann, A. Boucke, B.Perry, M. Ritter, M. Dalenbring, others?
- RTO meeting on Aeroelastic Benchmarking (July 1)

Configuration & Test Case Subcommittee Report: Test Case Selections

- Rectangular Supercritical Wing:
 - Steady Cases
 - $M = 0.825$, $\alpha = 2^\circ$ (RTO Case 6E23, TDT pt. 626)
 - $M = 0.825$, $\alpha = 4^\circ$ (RTO Case 6E24, TDT pt. 624)
 - Dynamic Cases
 - $M = 0.825$, $\alpha = 2^\circ$, $\theta = 1.0^\circ$, $f = 10$ Hz. (RTO Case 6E54, TDT pt. 632)
 - $M = 0.825$, $\alpha = 2^\circ$, $\theta = 1.0^\circ$, $f = 20$ Hz. (RTO Case 6E56, TDT pt. 634)
- Benchmark Supercritical Wing (Semi-Blind)
 - Steady Case
 - $M = 0.85$, $\alpha = 5^\circ$
 - Dynamic Cases
 - $M = 0.85$, $\alpha = 5^\circ$, $\theta = 1^\circ$, $f = 1$ Hz
 - $M = 0.85$, $\alpha = 5^\circ$, $\theta = 1^\circ$, $f = 10$ Hz
- HiReNASD
 - Steady (Static Aeroelastic) Cases
 - Mach 0.80, $Re = 7.0$ million, $\alpha = 1.5^\circ$, static aeroelastic, (exp. 132).
 - Mach 0.80, $Re = 23.5$ million, $\alpha = -1.34^\circ$, static aeroelastic, (exp. 250).
 - Dynamic Cases: forced oscillation at 2nd Bending mode frequency
 - Mach 0.80, $Re = 7.0$ million, $\alpha = 1.5^\circ$, (exp. 159).
 - Mach 0.80, $Re = 23.5$ million, $\alpha = -1.34^\circ$, (exp. 271).

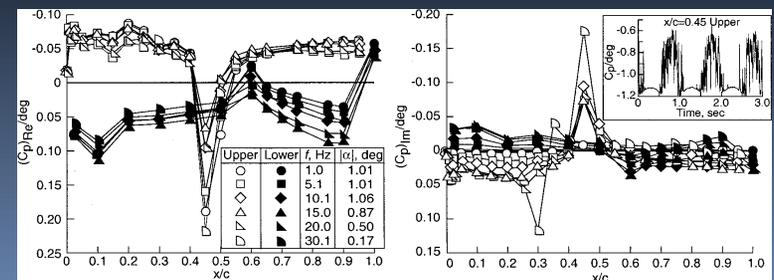
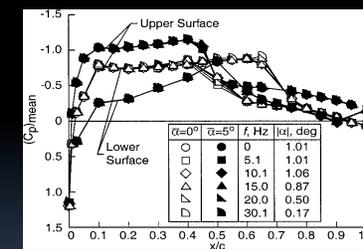
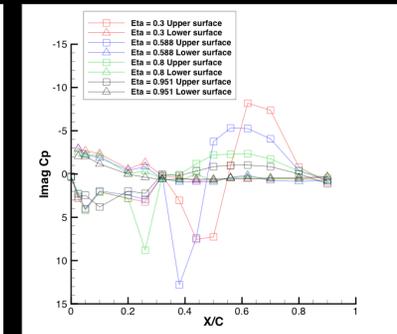
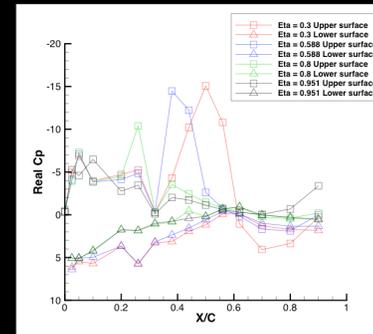
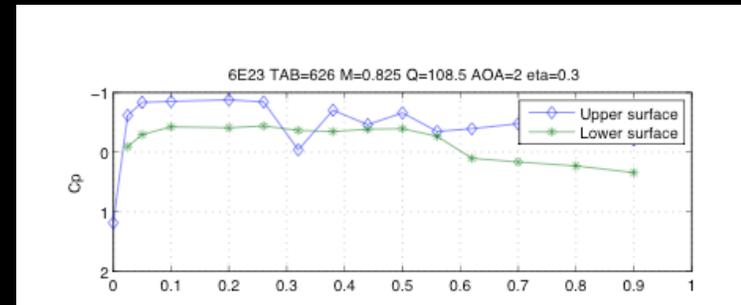
Gridding Guidelines Subcommittee Report

- **Gridding guidelines and rules from Drag Prediction Workshop and High Lift Prediction Workshop will be adopted as the initial guidelines for AePW.**
- **NASA is responsible for preparing IGES files:**
 - **Measured geometry should be used for all configurations**
 - **For RSW and BSCW IGES files will be generated with and without splitter plates**
 - **For HIRENASD, the IGES file supplied by Thorsten Hansen will be compared against files on Aachen website to establish baseline**
 - **IGES files should be ready by March 30**
- **Unstructured and structured grids will be constructed and made available to the participants.**
- **IGES files for RSW & BSCW are ready (March 30, 2011) for gridding**
 - **Volunteers to generate grids: Thorsten Hansen, Marilyn Smith, Eric Blades, Markus Ritter**
- **Initial analyses prior to IFASD will be conducted using new grid family:**
 - **RSW and BSCW (NASA)**
 - **HIRENASD (FOI Sweden)**

CONFIGURATION	REQUIRED CALCULATIONS				
	GRID CONVERGENCE STUDIES	STEADY CALCULATIONS		DYNAMIC CALCULATIONS	
RECTANGULAR SUPERCRITICAL WING					
Steady-Rigid Cases					
M = 0.825, $\alpha = 2^\circ$	C_L, C_D, C_M vs $N^{-2/3}$	C_p vs x/c	C_L, C_D, C_M	n/a	n/a
M = 0.825, $\alpha = 4^\circ$	C_L, C_D, C_M vs $N^{-2/3}$	C_p vs x/c	C_L, C_D, C_M	n/a	n/a
Forced-Oscillation-Rigid Cases					
M = 0.825, $\alpha = 2^\circ$, $\theta = 1^\circ$, excitation frequency = 10 Hz	TBD		n/a	Magnitude and Phase of C_p vs x/c at excitation frequency	Magnitude and Phase of C_L, C_D, C_M at excitation frequency
M = 0.825, $\alpha = 2^\circ$, $\theta = 1^\circ$, excitation frequency = 20 Hz	TBD		n/a	Magnitude and Phase of C_p vs x/c at excitation frequency	Magnitude and Phase of C_L, C_D, C_M at excitation frequency
BENCHMARK SUPERCRITICAL WING					
Steady-Rigid Cases					
M = 0.850, $\alpha = 5^\circ$	C_L, C_D, C_M vs $N^{-2/3}$	C_p vs x/c	C_L, C_D, C_M	n/a	n/a
Forced-Oscillation-Rigid Cases					
M = 0.850, $\alpha = 5^\circ$, $\theta = 1^\circ$, excitation frequency = 1 Hz	TBD		n/a	Magnitude and Phase of C_p vs x/c at excitation frequency	Magnitude and Phase of C_L, C_D, C_M at excitation frequency
M = 0.850, $\alpha = 5^\circ$, $\theta = 1^\circ$, excitation frequency = 1 Hz	TBD		n/a	Magnitude and Phase of C_p vs x/c at excitation frequency	Magnitude and Phase of C_L, C_D, C_M at excitation frequency
HIRENASD					
Static-Aeroelastic Cases					
M = 0.800, $\alpha = 1.50^\circ$, Re = 7.0 million	C_L, C_D, C_M vs $N^{-2/3}$	C_p vs x/c, vert displ* vs x/c, twist* vs x/c	C_L, C_D, C_M	n/a	n/a
M = 0.800, $\alpha = -1.34^\circ$, Re = 23.5 million	C_L, C_D, C_M vs $N^{-2/3}$	C_p vs x/c, vert displ* vs x/c, twist* vs x/c	C_L, C_D, C_M	n/a	n/a
Forced-Oscillation-Aeroelastic Cases					
M = 0.800, $\alpha = 1.50^\circ$, Re = 7.0 million, excitation frequency = 2 nd bending mode frequency	TBD		n/a	Magnitude and Phase of C_p vs x/c at excitation frequency	Magnitude and Phase of C_L, C_D, C_M at excitation frequency **
M = 0.800, $\alpha = -1.34^\circ$, Re = 23.5 million, excitation frequency = 2 nd bending mode frequency	TBD		n/a	Magnitude and Phase of C_p vs x/c at excitation frequency	Magnitude and Phase of C_L, C_D, C_M at excitation frequency **

Experimental Data & Uncertainty Subcommittee Report

- Rectangular Supercritical Wing
 - Static data 6E23, 6E24 extracted from RTO CD
 - Dynamic data for test cases 6E54, 6E56
- Benchmark Supercritical Wing
 - Semi-blind, so no data will be released beyond that appearing in Journal article
 - Time history data available to AePW for uncertainty analyses &



Experimental Data & Uncertainty Subcommittee Report

■ HiReNASD

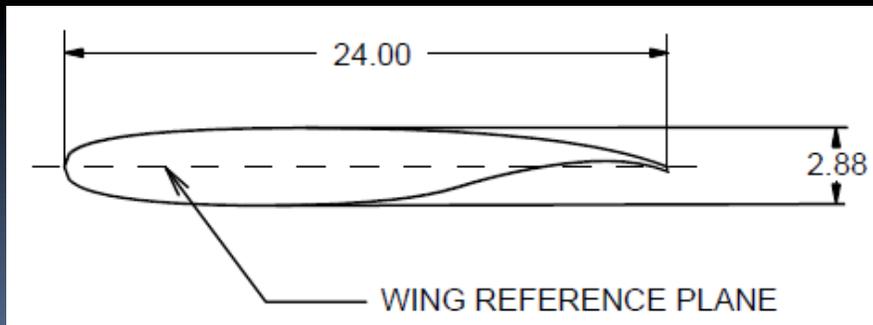
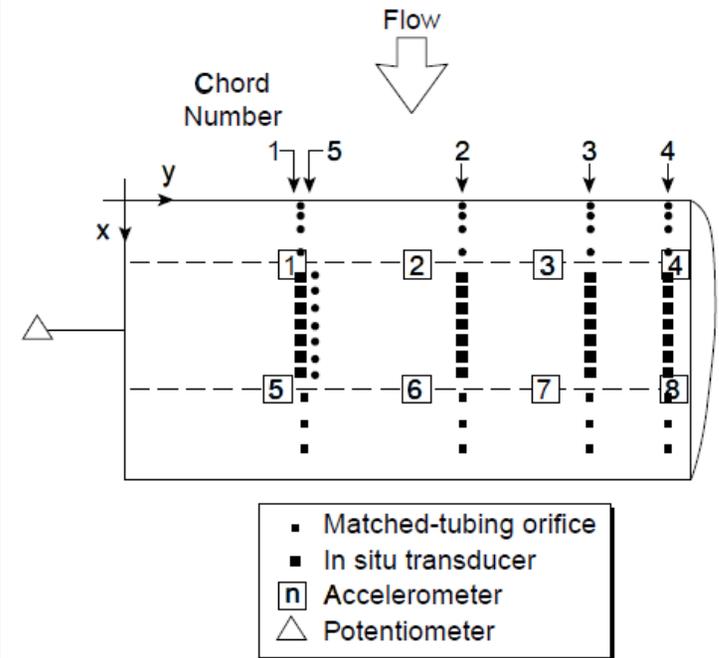
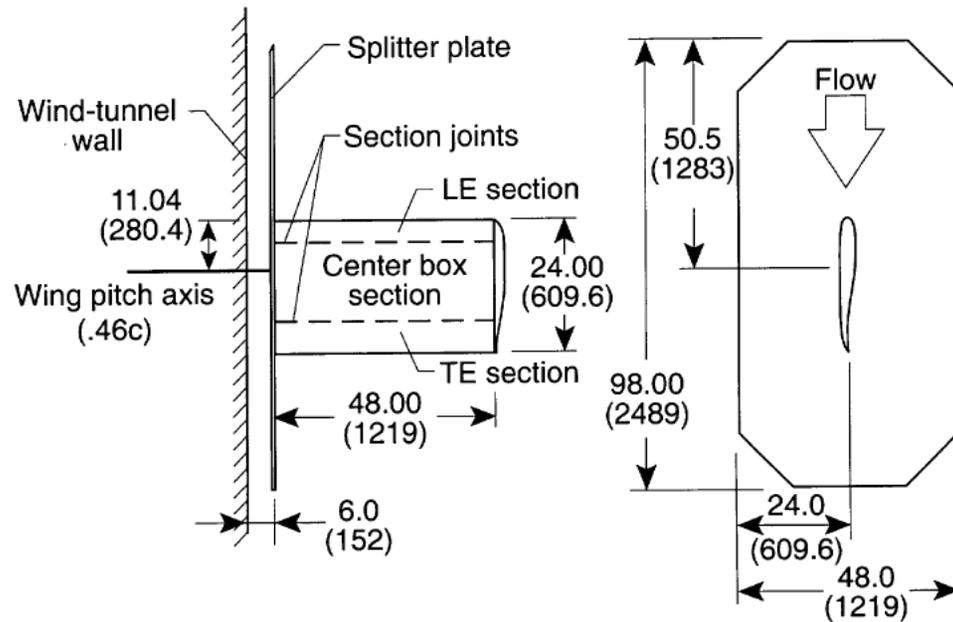
- Time histories being analyzed by Aachen University & NASA
 - Pressure data
 - Balance data
 - Accelerometers
 - Forcing functions
- Processed data being analyzed for displacements
 - Stereo pattern tracking
 - Strain gauges
- Wind-off data sets also being analyzed
- Treatment of uncertainty in experimental data- under discussion and debate

Case 1 Selection Rationale

Rectangular Supercritical Wing (RSCW)

- Cases chosen to focus on the steady and unsteady aerodynamic solutions and their variation.
- Mach 0.825 generates transonic conditions with a terminating shock; highest Mach number with forced transition
- Steady Data: Two static angles of attack chosen
 - $\alpha = 2.0^\circ$ generates a moderate-strength shock with some potential for shock-separated flow; corresponding forced oscillation data exists.
 - $\alpha = 4.0^\circ$ generates strong shock with greater potential for shock-separated flow .
- Unsteady Data: Two forced oscillation frequencies chosen to evaluate methods abilities to distinguish frequency effects.
 - Non-zero mean AoA introduces a wing loading bias for which code-to-code comparisons can be accomplished.

RSW Model Layout and Airfoil



Experimental data acquired in R-12 @ $Re = 4$ million/ft (8 million based on wing chord), $Mach=0.825$

RSW Model Layout and Airfoil

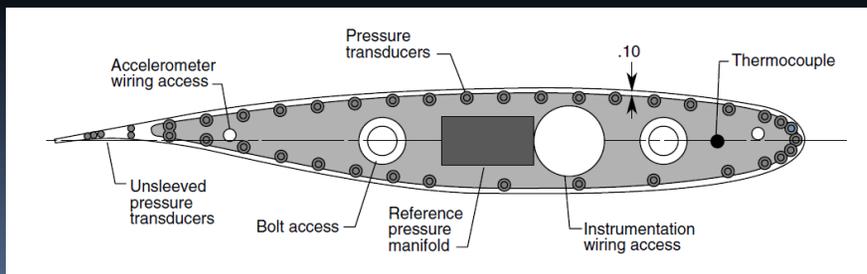
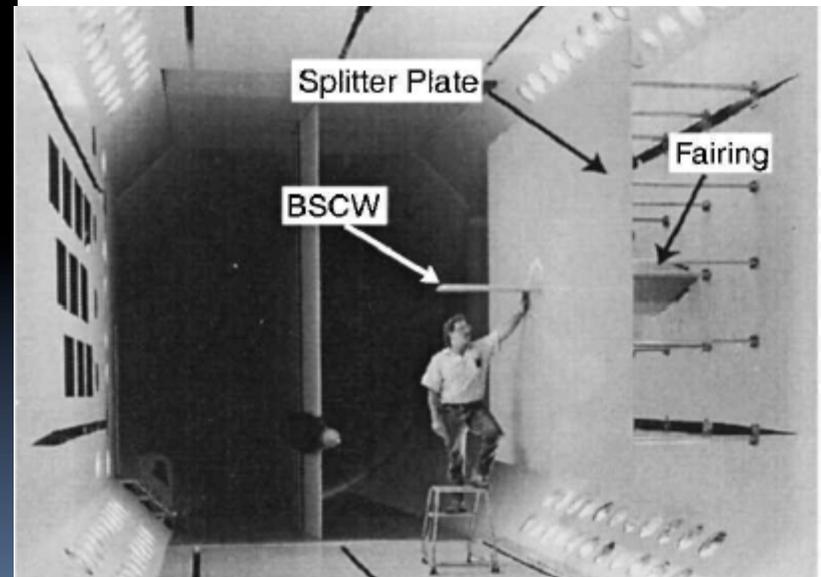
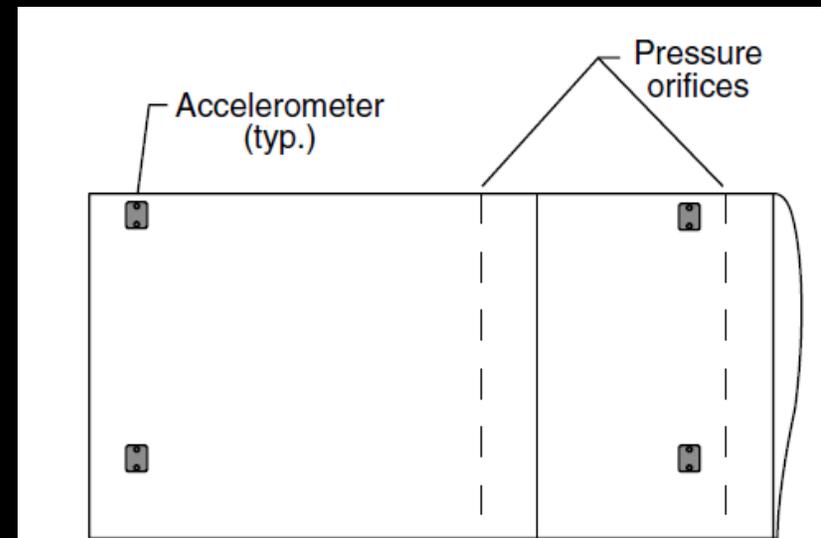
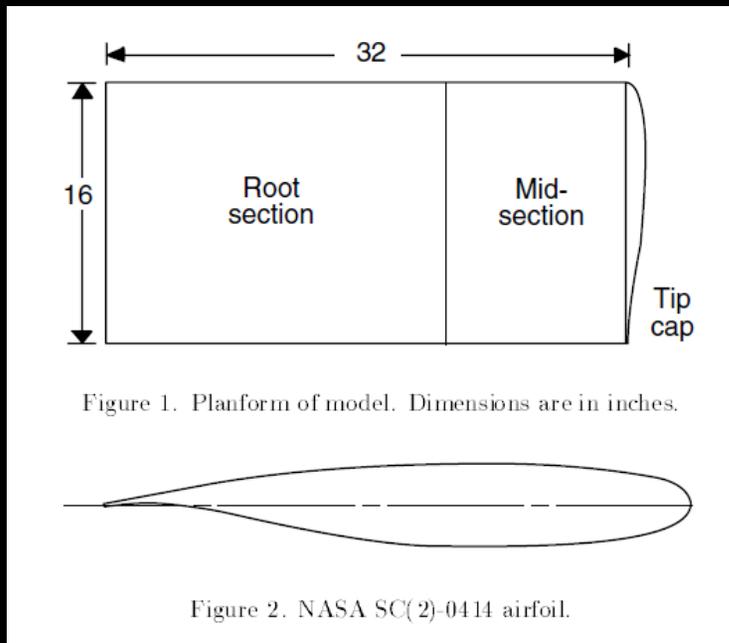


Case 2 Selection Rationale

Benchmark Supercritical Wing (BSCW)

- Highly nonlinear aerodynamic phenomena.
 - Known shock-separated transient flow.
 - Relatively obscure data that serves as a virtually blind test case for the methods.
- Better data detail and insight than for RSCW.
 - Statistical and time-history data are available for comparison.
 - Unfortunately only one span station of data.
 - Model could be retested for future workshops.

BSCW Geometry and Test Configuration



Experimental data acquired in R-134a @ $q = 200$ psf, $Re = 5.3$ million/ft. (7 million based on wing chord), Mach=0.85 24

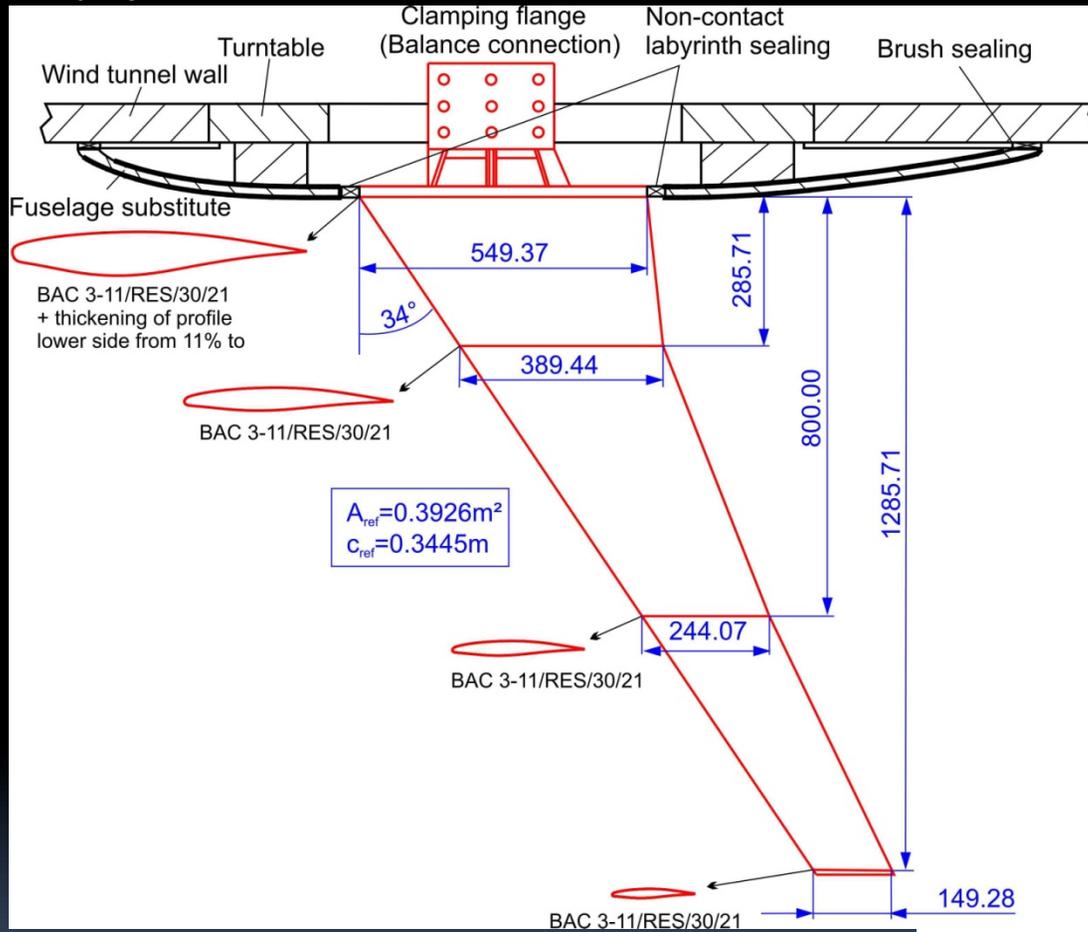
Case 3 Selection Rationale

HIRENASD Wing

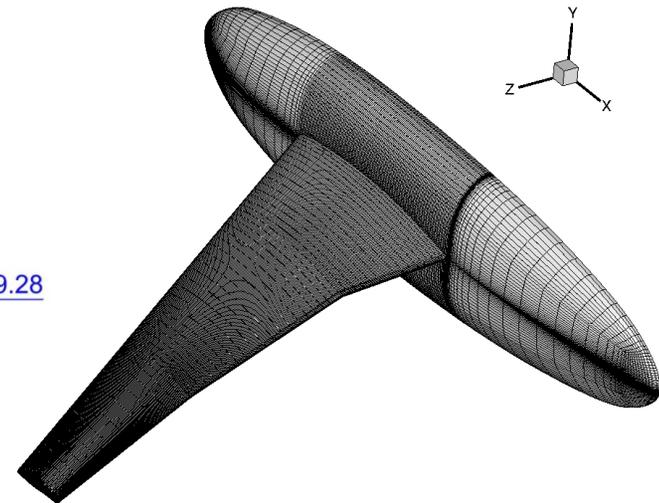
- Aircraft-representative geometry, rather than “unit problem”
- Initial test for fully coupled aeroelastic analysis.
- Steady cases demonstrate prediction capabilities for static aeroelastic problems.
- Dynamic cases demonstrate structural dynamics coupling with unsteady aerodynamics techniques.
 - Relatively weak aeroelastic coupling make it a good entry-level aeroelastic test case.

HIRENASD Geometry

(<https://heinrich.lufmech.rwth-aachen.de/en/windtunnel-assembly>)

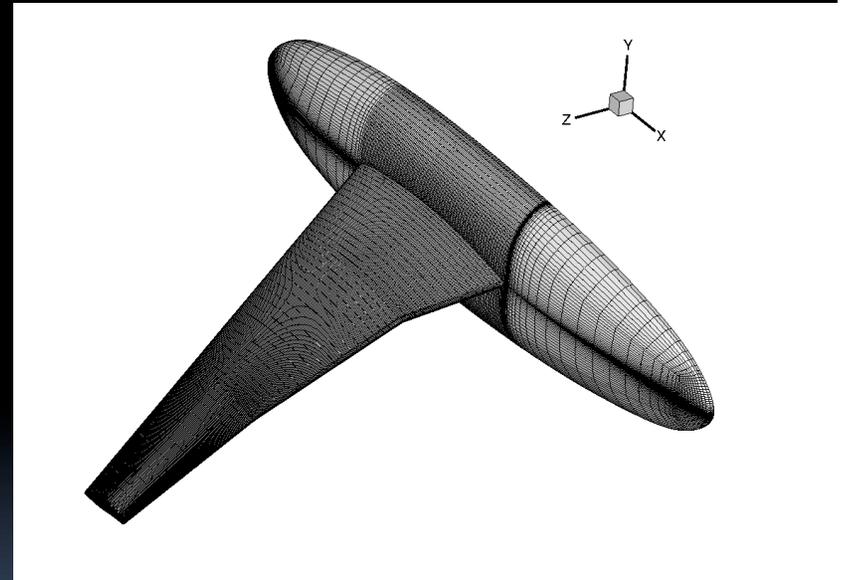


**Mach 0.80, $Re = 7.0$ million
and $Re = 23.5$ million**



High Reynolds Number Aero-Structural Dynamics (HIRENASD) Wing

- 3-D aeroelastic wing with generic fuselage model.
 - Steady and forced (structural resonance) oscillation testing
 - Moderate and high Reynolds number data.
- Well known geometric and structural properties.
- Data includes balance forces for integrated load comparisons, mean and fluctuating pressure data, and surface deformation data from optical and strain measurements during testing.



Participant Information Sources

- Organizing committee website:
 - <https://c3.ndc.nasa.gov/dashlink/projects/47/>
- Workshop website, open for public viewing, member postings:
 - <https://c3.ndc.nasa.gov/dashlink/projects/39/>
- Links to:
 - HIRENASD website (German and English languages)
 - <http://www.lufmech.rwth-aachen.de/HIRENASD/>
 - <https://heinrich.lufmech.rwth-aachen.de/index.php?lang=en&pg=home>
 - NASA White Paper reviewing experimental data sets
 - http://ntrs.nasa.gov/archive/nasa/casi.ntrs.nasa.gov/20100016316_2010017232.pdf
 - 2011 International Forum on Aeroelasticity & Structural Dynamics
 - <http://www.ifasd2011.com/>
 - Fun3D
 - <http://fun3d.larc.nasa.gov/>
 - Drag and High-Lift Prediction Workshops
 - <http://aaac.larc.nasa.gov/tsab/cfdlarc/aiaa-dpw/>
 - <http://hiliftpw.larc.nasa.gov/>

Mapping configurations to Activities & Organizations

	NASA	NASA	NASA	OTO	OTO	AEPW	AEPW	AEPW
	SFW-AeroD, 2010	SFW-AeroD, 2011	SFW-AeroD, 2012-14	AVT 203, 2011-12	AVT 203, 2013-2014	1	2	3
AGARD 445.6	Principal config	Secondary config						
RSW		Principal config				Principal config		
BSCW		Principal config				Principal config		
HiRENASD, Case Set 1		Principal config		Principal config		Secondary config	Principal config	
HiRENASD, Case Set 2			Principal config	Principal config			Principal config	
TBD Aeroelasticity Benchmark			Principal config		Principal config			Principal config

Self-rating
By each
Organization:

- Principal config
- Secondary config